

# Variable Speed Motor Control

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Variable Speed Motor Control

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A COMPARATIVE STUDY OF  
VARIABLE SPEED MOTOR CONTROL

A THESIS

PRESENTED BY

AUGUST FRY  
CHARLES BAKER

TO THE

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## A COMPARATIVE STUDY OF VARIABLE SPEED CONTROL.

There has been for a number of years and increasing demand for variable speed motors for the direct driving of machinery. It is the general opinion that the great bulk of machinery in the future is to be driven by electric motors rather than belt drivers. There are a number of important conditions that are essential and which must be met in order that variable speed motors shall come into general use. Among these may be mentioned: nonspinning under excessive loads; large range of speeds; speed to be constant at all loads where adjusted to any desired speed; compactness; simple mechanical construction; reversibility; lightest possible weight; and high efficiency under average loads.

The different methods by which variable speed of motors is obtained are as follows:-

- 1st. Rheostat in the armature circuit.
- 2nd. Rheostat in the field circuit.
- 3rd. Combination of 1st. and 2nd.
- 4th. Multivoltage system.
- 5th. Variations of air gap, or variation of magnetic reluctance in the field circuit.
- 6th. Interpole method.

By introducing a variable resistance in the armature circuit, thus controlling the voltage impressed on the armature terminals, a variation in speed from zero to a maximum may be obtained.

But this is a very wasteful method, and, furthermore, for a



For a given position of the rheostat the speed will vary according to the current consumed. If the torque required of the motor is increased, the armature current will increase and the speed will diminish, although the rheostat position remains unchanged. The large loss of power due to the rheostat, the  $C^2R$  loss, is a clean loss, and the rheostat, which is usually of large proportions, make the method inefficient and undesirable.

The method of introducing resistance in the field circuit is far more efficient, involving only the very slight loss of the shunt adjusting rheostat. As the current is decreased the field is decreased, and the C. E. M. F. in the armature is decreased. As the C. E. M. F. of the armature decreases the current flowing through the armature will increase, causing an increase of speed. The objection to the method is that violent sparking at the commutator is encountered with a variation of speed of from 30% to 40% above normal.

The multi voltage motor supplies the motor with a number of voltages necessary to obtain the range of speed. The range in voltage may be obtained by means of a number of generators in series; a large generator and a set of boosters; or a storage battery with an end cell switch. This method is efficient for all ranges of speed and load, but requires complicated wiring and accessories.

The variation of magnetic reluctance in the field circuit is obtained by two methods. First, by a movable soft iron core



in a hollow pole-piece. Second, by means of the same device, the influence of the field poles. This is accomplished by any of the proceeding in that a wide range of speed is obtainable, good efficiency at ordinary loads, and no other little apparatus outside of the motor itself.

The inter-pole method of speed variation can be obtained in a shunt motor, between the poles of which are placed a series of poles, the windings of which are in series with the armature. The speed is controlled by a rheostat in the shunt field circuit. The method is simple and highly efficient.

Emulating the successful records of the foregoing methods, and the multivoltage system, three motors were obtained and which to work. These were the Stone, Lincoln and Interpole, which are successful, variable speed motors on the market. In each of them a rheostat was used which enabled us to make a comparative study of the qualities essential to successful variable speed control.

The Inter-Pole Motor is essentially a shunt motor obtaining speed variation by means of a rheostat in field circuit. It has, however, one or two unique features of construction added by means of which a large range of speed is obtainable. One of these features is the presence of the segments in the commutator, the cutting down the reactance voltage, and the other is the introduction of auxiliary poles which are located between the main poles. These poles are small compared with the main poles and are provided with coils connected in series with the armature. Owing to this latter fact weakening of the field on a sudden



produce the required commutating field of excitation independent of the main field which is decreased as the speed is increased. The effect of the auxiliary pole is the same regardless of the direction of the rotation, because when the current is reversed in the armature it is also reversed in the auxiliary poles. Points in favor of this motor are its compactness, its compactness and absence of accessories. The armature is carried on ball bearings, thus by reducing friction to a minimum.

The Lincoln motor is an ordinary shunt motor, the shunt field winding being connected in series. Speed variation is obtained by withdrawing the armature from the influence of the field poles. As the armature, which is slightly conical in shape, is withdrawn the magnetic resistance, due to increase in air gap, is increased, thus by decreasing the useful magnetic flux and thus increasing the speed. Special commutating poles are provided under the face of which the armature comes as it is withdrawn into its positions of high speed. The full field strength is used for all speeds, thereby eliminating the undesirable feature of field distortion.

A hand wheel is used in connection with a screw mechanism to move the armature laterally and by means of this wheel it is possible to get an infinite variety of speeds from the lowest to the highest. The magnetic pull of the armature is carried on ball thrust bearing, which reduces all friction. The brushes





are carried on the turnst bearing, armature and commutator can move together, and there is no relative lateral motion between the commutator and the brushes.

The Stowe motor is a shunt motor having pole\* piece, the ends of which are movable. The poles are composed of a pole shoe of common form integrally connected with a cylindrical shell, over which the magnetizing coils are wound, and with which is a solid core of high permeability and of cross section relatively large as compared with the conducting area of the inclosing shell. By means of a hand wheel this inner core is adjustable in any direction radial to the center of the armature, and is so proportioned that a slight variation in its position within the magnetized shell produces a considerable difference in the reluctance of the magnetic circuit of which the plunger forms a part. When the plunger is so adjusted that the inner end comes in contact with the pole shoe the magnetic circuit is most complete and of minimum reluctance, and since the magnetomotive force remains constant the volume of the magnetic flux becomes a maximum and the speed a minimum or normal. As the plunger is drawn away from contact with the pole shoe ~~xxx~~ ~~xxx~~ ~~xxx~~ a column of air is interposed which gradually increased the reluctance of the magnetic circuit as long as the plunger continues to be withdrawn. As the plunger is moved the gap between the pole face and the armature remains constant, the air gap inside the pole being the one which is varied, and the design of the pole piece and plunger is such that



as the total effective magnetic field is diminished by outward movement of the plunger the remaining magnetic flux is forced more and more in the direction of the pole tips, thus concentrating magnetic flux at all times of sufficient intensity to insure sparkless commutation.

The apparatus used for the tests were an ammeter, a field meter, a voltmeter for the main line voltage, and a tachometer voltmeter. Load was applied to the motor by means of a spring brake upon a charged pulley. The power supplied to the motor under test was developed in a 15 H. P. Westinghouse generator, driven by a direct coupled Crocker-Whelan motor. The D. H. P. impressed on the motor terminals was kept constant at 110 volts by varying the speed of the generator. A small set of scales were used with graduations to 1/50 of a pound.

The first set of runs was taken with the lowest rated speed, as indicated on the name plate. The load was increased from zero to about fifty per cent over load. During these runs readings were taken of the armature current, field current, tachometer and scale, and from the data obtained the developed horse power (D. H. P.); the electrical input; and the efficiency were obtained. By adding the armature and field current and multiplying by the constant voltage of 110 volts the electrical input was obtained. The D. H. P. was obtained from the scale.

$$D. H. P. = \frac{2\pi n \ell w}{53000}$$



where  $n = \text{r. r.} \therefore l = \text{brake h.p.} \therefore \eta = \frac{\text{brake h.p.}}{\text{input h.p.}}$   
~~efficiency~~. Efficiency can be calculated by the following  
 equation:

$$\text{Efficiency} = \frac{343 \times \text{B. H. P.}}{\text{I. P. put}}$$

The above set of tests was taken on the three machines and was  
 taken in both directions of rotation. Then the results were  
 related to the first value, and then to the highest value, etc.  
 a similar set of runs were made.

The data was tabulated on separate sheets, a check list being  
 made of each. In the International motor each day, load speed and  
 efficiency curves plotted. In the inclined plane motor, also,  
 the average of the two runs was plotted.

Another test made upon the motor was with the P. D. constant  
 but at a constant value and the speed was varied.  
 Full rated load and half load runs were taken in both directions  
 of rotation on each of the motors. From this test it was  
 able to obtain an idea of the <sup>efficiency</sup> of the various machines  
 under load, with variation of speed.





# Interpole Factor.

Low Speed.

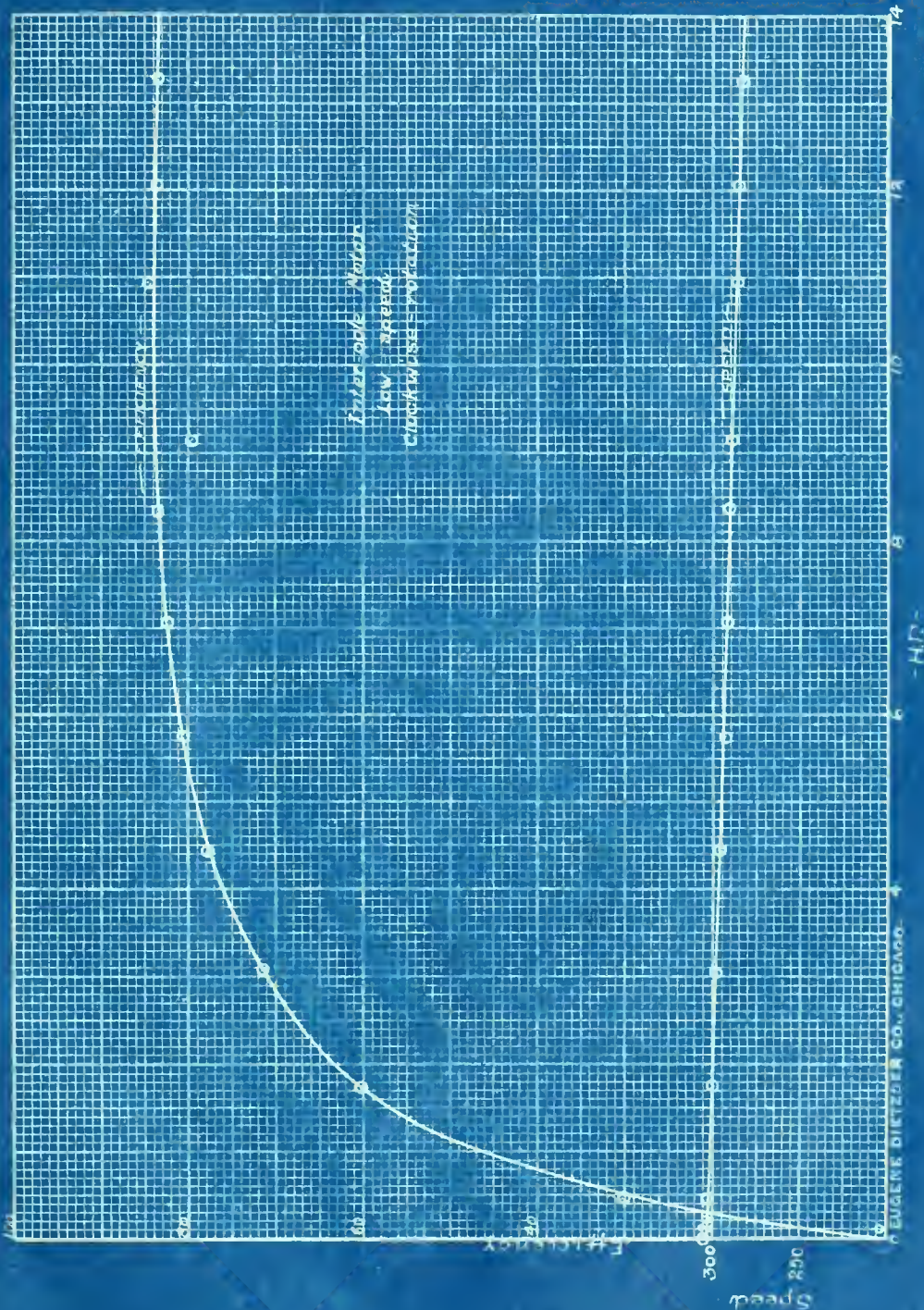
Clockwise Rotation.

Ia.	If.	Motor Input.	Speed.	Wt.	H. P.	Eff.
5.0	4.415	1154	306	3.40	.43	6.7
15.0	4.37	3134	304	14.3	1.71	10.5
24.6	4.35	5173	300	26.3	3.03	12.5
34.1	4.32	4223	299	37.3	4.32	13.5
43.8	4.29	7233	295	50.1	5.77	14.5
53.3	4.26	10333	294	62.1	7.04	15.2
62.5	4.23	7453	293	74.1	8.52	15.5
72.3	4.24	5563	291	86.3	9.75	15.5
82.3	4.22	9237	290	98.3	10.92	15.5
92.9	4.21	10731	289	110.3	12.02	15.7
104	4.225	11302	288	122.3	13.21	15.7
115.	4.225	13112	282	134.3	14.50	15.5
126.1	4.225	14338	283	145.3	15.74	15.5
133.4	4.225	15436	281	157.3	17.00	15.5

10.5	4.22	750	283	0.	0.	6.5
17.7	4.27	1096	286	1.2	3.75	10.1
18.	4.25	3227	284	14.3	5.75	12.1
24.7	4.23	5123	282	26.3	8.06	13.0
34.7	4.22	4321	283	37.3	9.31	13.5
44.3	4.20	5553	285	50.3	10.50	14.5
54.2	4.18	3421	284	62.3	11.74	15.5
64.0	4.17	7493	292	74.3	13.52	16.0
73.3	4.13	3554	292	86.3	15.15	17.3
83.3	4.24	3318	290	98.3	16.92	18.0
94.1	4.11	10303	297	110.3	18.12	18.3
105.	4.10	12010	283	122.3	19.30	18.5
116.0	4.095	13210	283	134.3	20.30	18.5
127.3	4.066	14504	284	145.3	21.50	18.7
139.5	4.05	15790	184	157.3	22.73	18.8

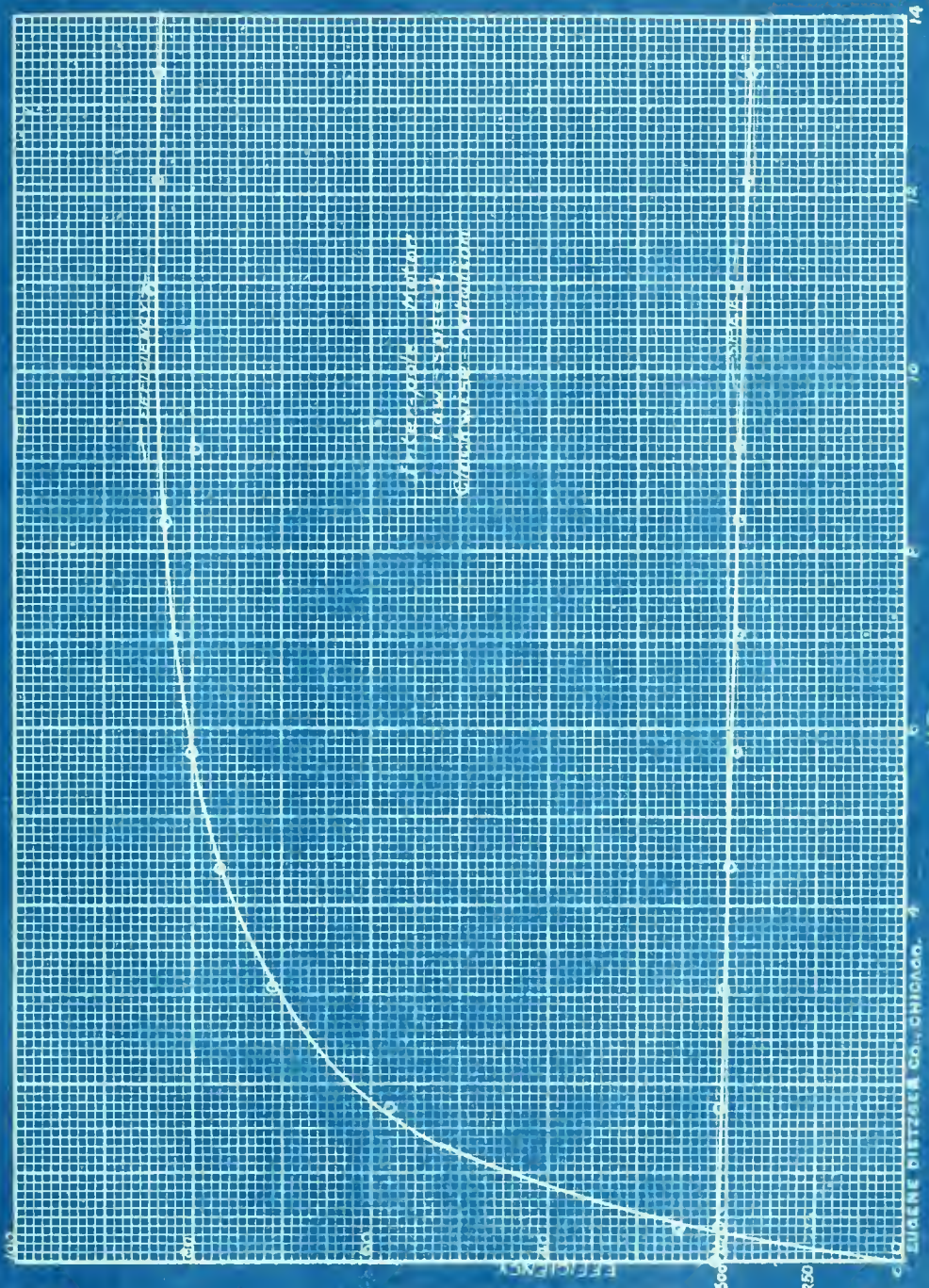
2--110 Volts











EUGENE DIETZGEN CO., CHICAGO.



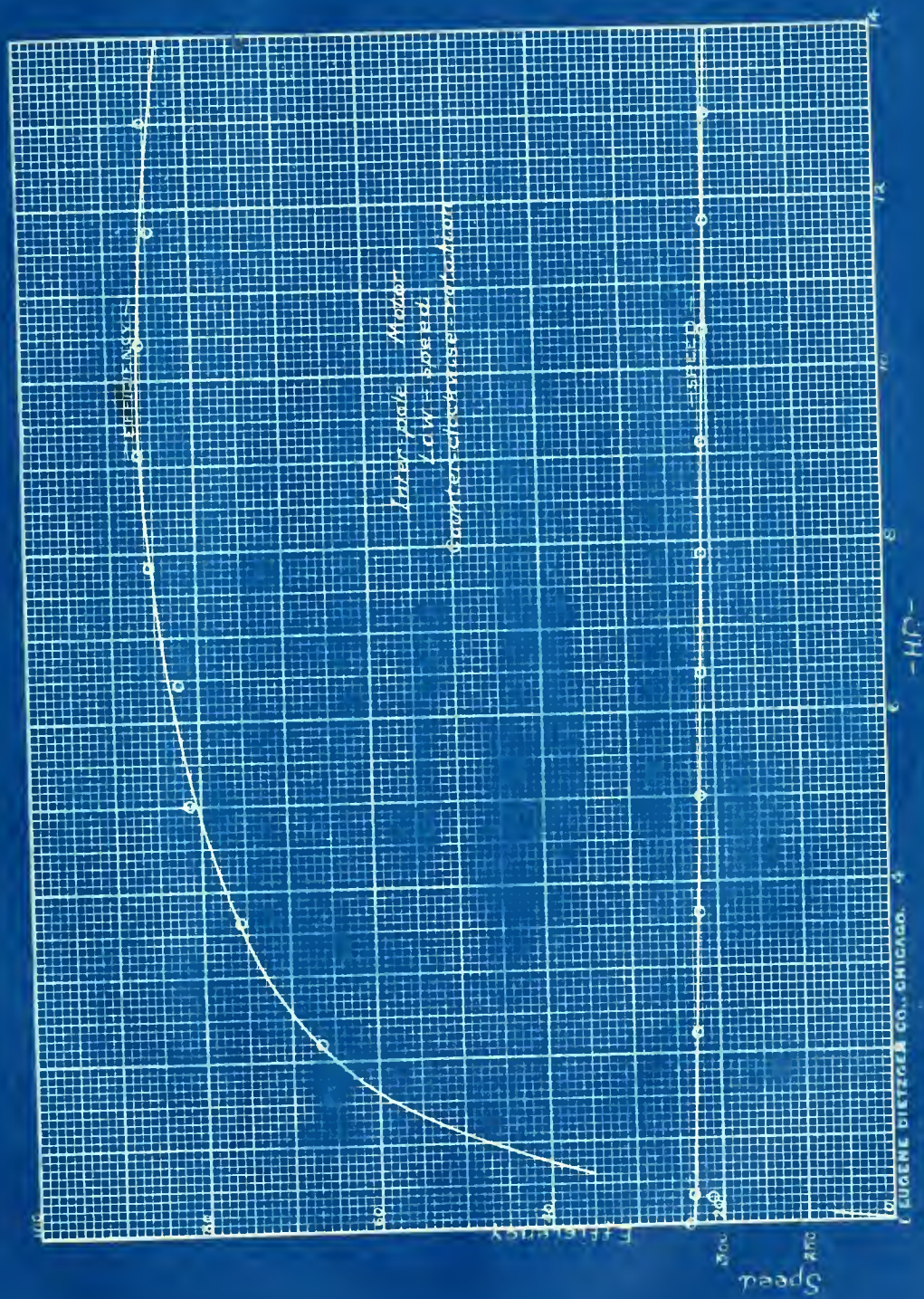
# Interpole Motor.

1a.	Low Speed	Watt	Counter Clock		100 R. per min.	
	If.		Speed	ft.	H. P.	Eff.
		Input.				
36;						
5.0	4.84	786	312	0.0	0.	0.
6.7	4.23	1210	312	4.2	.5	32.2
12.6	4.22	2710	306	12.3	2.2	72.5
22.4	4.20	3536	304	30.8	3.57	72.4
32.0	4.20	4342	304	42.3	4.97	70.5
47.7	4.19	5707	301	54.8	6.38"	62.7
57.4	4.18	6773	298	66.8	7.61	62.3
67.5	4.17	7884	297	78.8	8.44	64.0
77.4	4.17	8972	293	90.8	10.34	64.
87.2	4.14	10047	292	102.8	11.51	64.7
97.4	4.13	11168	293	114.8	12.87	65.2
109	4.12	12445	292	126.8	14.12	64.0
119.2	4.09	13561	291	138.8	15.4	64.0
130.5	4.08	14803	289	150.8	16.06	64.3
142.	4.06	16066	288	162.8	17.89	62.2
3.2	4.19	813	321	0.	0.	0.
5.8	4.18	1097	318	2.6	.315	21.4
12.8	4.15	2491	313	18.8	2.24	66.5
22.6	4.14	3301	312	30.8	3.33	75.3
37.8	4.12	4311	309	42.3	5.05	61.7
48.8	4.11	5320	306	54.8	6.42	62.3
57.7	4.10	6728	305	66.8	7.78	65.5
67.5	4.09	7874	304	78.8	9.13	63.5
78.4	4.07	9071	301	90.8	10.4	66.0
89.9	4.06	10335	300	102.8	11.74	64.8
100.	4.05	11445	298	126.8	14.45	65.4
125.3	4.04	14007	295	132.8	15.6	65.2
135.5	4.01	15343	292	150.8	16.3	61.75

22-110 Volts





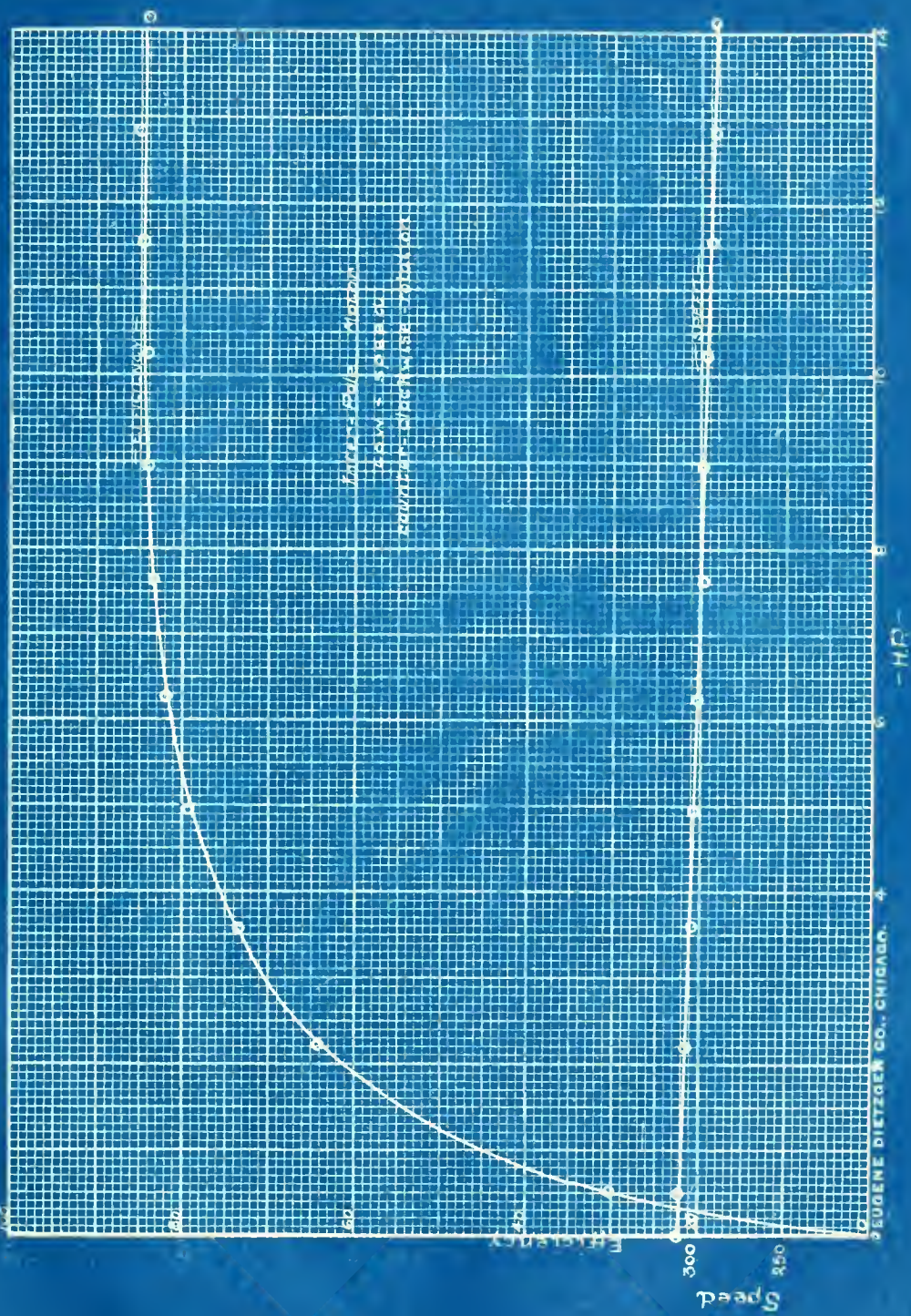


-HP-

EUGENE DIETZGEN CO., CHICAGO.







1/2 HP Motor  
 Efficiency vs. Speed

-HP-

EUGENE DIETZGEN CO., CHICAGO.



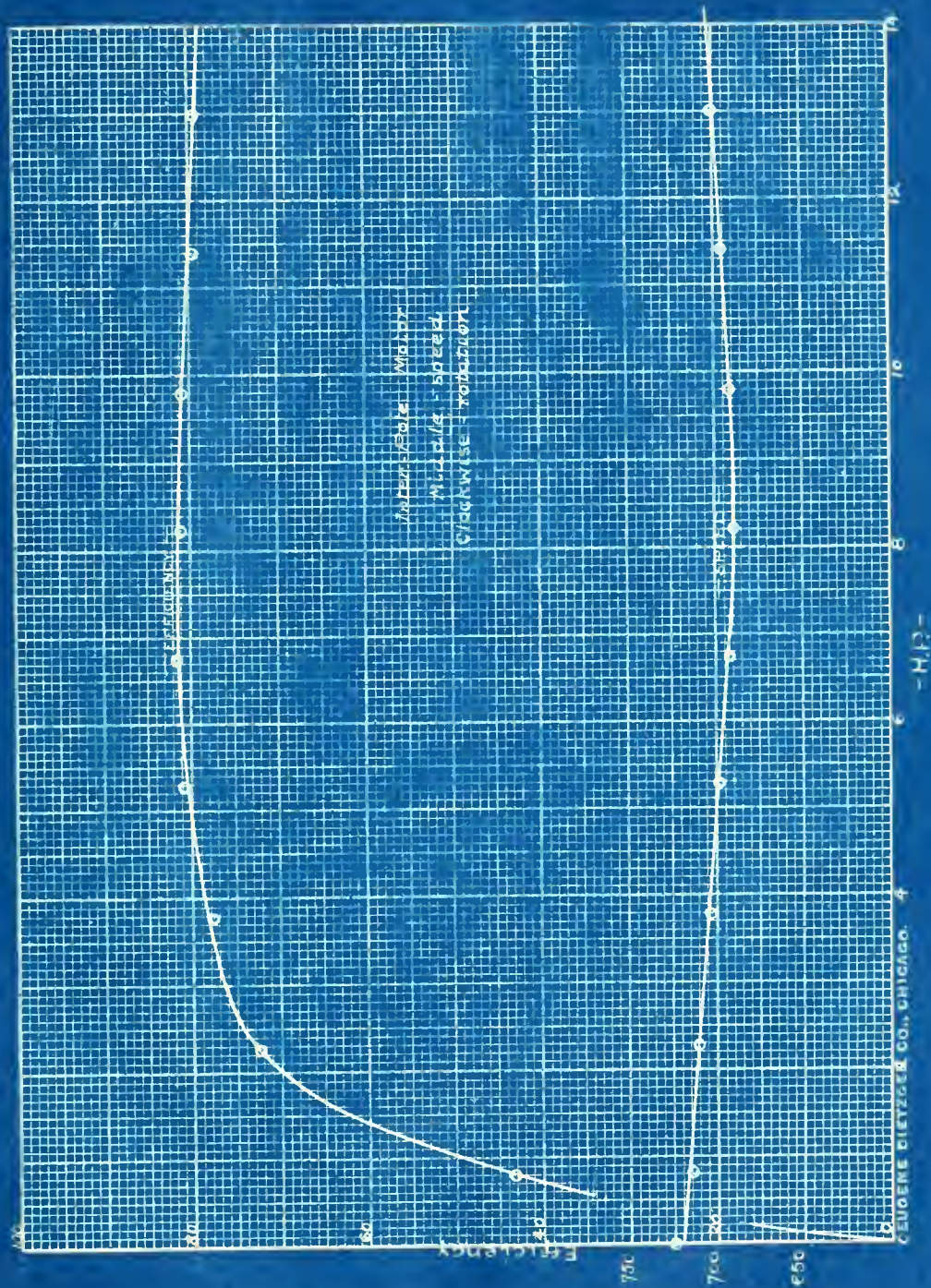
# Interpole 1041.

Middle speed 31.4 m/sec P t 11 m.

Id.	If.	Input	Speed	WT.	R.R.	Eff.
2.3	1.26	380	725	0.	0.	0.
11.3	1.26	1381	713	3.1	2.507	45.3
20.1	1.26	2340	710	8.3	3.23	72.4
31.7	1.23	3335	703	14.8	3.78	77.3
43.0	1.23	4333	697	20.8	5.23	81.
55.0	1.23	5133	693	23.3	3.73	81.3
67.3	1.23	7374	687	32.3	3.23	81.
80.9	1.23	9033	692	33.3	9.79	80.3
93.0	1.23	10393	697	44.3	11.4	73.3
109.5	1.23	12133	702	50.8	13.01	79.3
123.6	1.23	15734	702	56.8	14.53	79.1
139.7	1.23	15503	707	32.3	15.3	77.3
10.4	1.24	1290	714	0.	.83	45.3
21.1	1.24	2457	704	3.2	2.26	38.3
33.	1.24	3766	690	8.8	3.78	74.9
44.8	1.24	5034	694	14.3	5.23	77.3
56.7	1.24	6373	690	20.8	3.75	79.1
69.4	1.24	7770	688	26.8	3.24	79.0
82.5	1.24	9211	683	32.3	9.72	73.7
93.0	1.24	10916	685	33.3	11.43	79.3
110.	1.24	12236	683	45.3	12.39	77.3
124.9	1.24	13375	680	50.8	14.1	73.0
140	1.24	15533	678	56.8	15.53	74.5

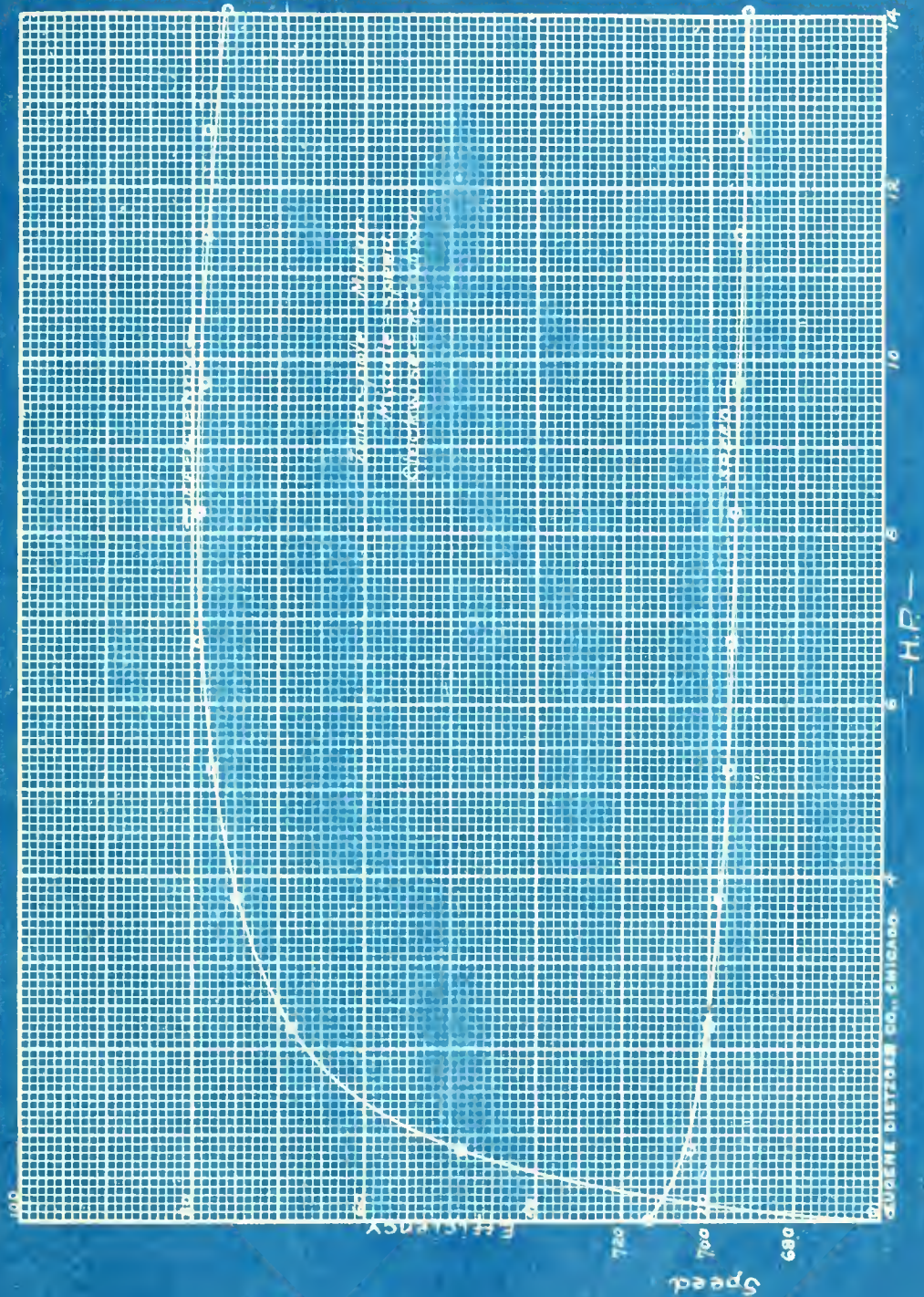












QUINCY DISTRICT CO., CHICAGO

-HP-



# Interpole

Middle Speed

C. Clockwise Rotation

Watt

Ia.	If.	Input	Speed	Wt.	H. P	Eff.
3.6	1.31	540	725	0	0	0
11.8	1.31	1441	723	3.56	.38	50.8
21.6	1.315	2520	715	8.8	2.4	71.
33.6	1.315	3840	715	14.8	4.03	78.4
45.4	1.315	5138	717	20.8	5.67	82.4
53.1	1.3	6534	720	26.8	7.35	84.0
70.6	1.295	7908	722	32.8	9.01	85.
83.1	1.295	9284	722	38.8	10.63	85.9
96.1	1.3	10714	717	44.8	12.27	85.4
11.05	1.295	12298	714	50.8	13.84	84.1
12.18	1.295	13541	708	56.8	15.34	84.3
135.0	1.295	14993	703	62.8	16.8	83.7

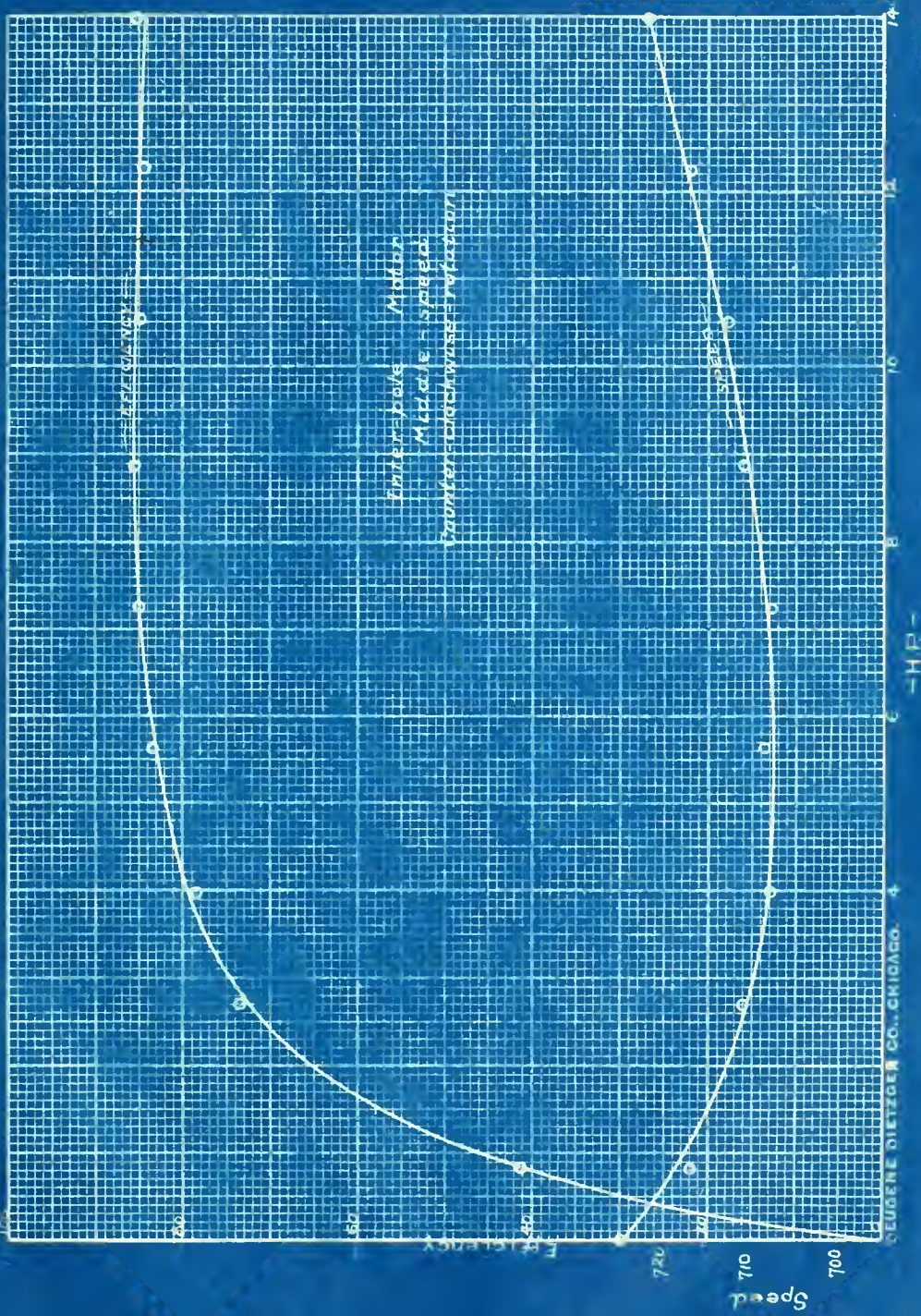
E---110 Volts

5.	1.295	465	725	0	0	0
10.7	1.295	1519	717	2.98	.314	41.1
23.6	1.295	2739	711	9.98	2.7	73.75
33.2	1.29	3795	708	14.8	3.99	78.5
44.4	1.29	5026	709	20.8	5.62	83.5
56.5	1.29	6357	708	26.8	7.23	84.9
69.5	1.29	7787	711	32.8	8.89	85.2
829	1.29	9261	713	38.8	10.54	84.9
97.5	1.295	10868	717	44.8	12.27	84.3
110.7	1.29	12320	722	50.8	13.99	85.3
124.7	1.29	13955	717	56.8	15.62	83.5
139.	1.235	15572	713	62.8	17.02	82.5

1890

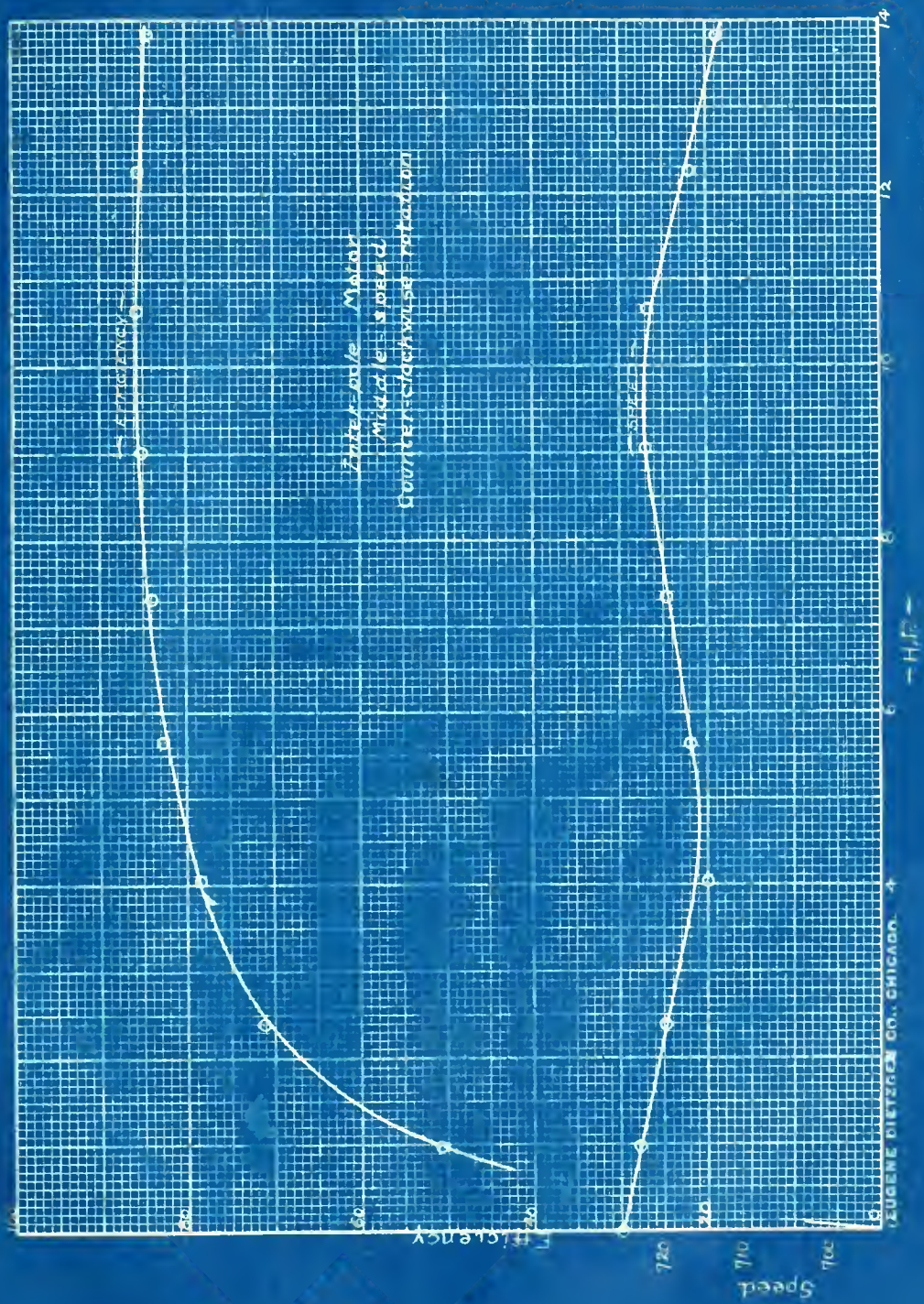
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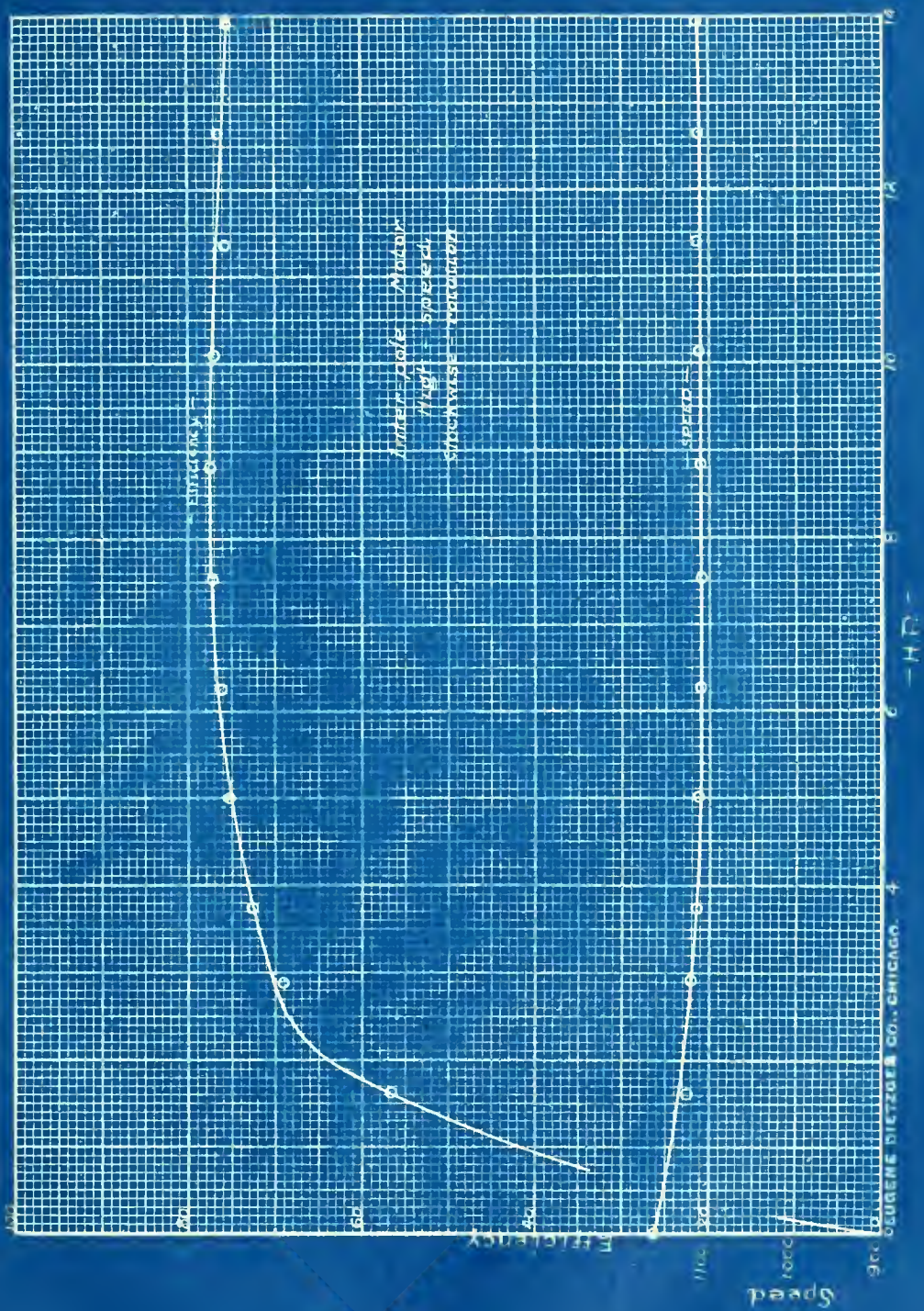
# Interpole Motor.

High Speed			Clockwise Rotation.			
Ia.	If.	Watt Input	Speed	Wt.	H.P.	Eff.
5.3	.83	453	1160	0.	0.	0.
16.1	.83	1865	1125	3.38	1.55	54.5
23.7	.83	2398	1117	5.03	2.47	63.4
34.1	.83	3342	1110	8.3	3.72	72.3
44.4	.83	4975	1110	11.8	4.99	74.2
54.2	.83	6253	1109	14.8	6.25	77.0
64.0	.83	7131	1108	17.3	7.55	78.4
76.0	.83	8451	1102	20.8	8.3	77.3
86.3	.83	9584	1117	23.2	10.1	75.0
99.0	.83	10931	1125	26.3	11.5	73.3
112.	.83	12411	1130	29.3	12.7	71.0
124.0	.83	13930	1125	32.8	14.07	73.
135.5	.83	14996	1113	35.6	15.17	75.5
3.4	.835	465	1130	0.	0.	0.
16.6	.835	2137	1125	3.89	1.63	53.5
27.7	.835	3138	1120	6.00	2.9	62.0
34.1	.835	3342	1115	8.3	3.74	70.7
44.4	.835	4975	1113	11.8	5.02	75.4
54.8	.835	6119	1110	14.8	6.23	73.4
65.6	.835	7707	1110	17.3	7.55	71.2
74.3	.835	8484	1110	20.8	8.31	77.60
88.2	.835	9793	1113	23.2	10.1	77.0
101.5	.835	11256	1117	26.3	11.59	75.7
110.	.835	12501	1113	29.3	12.66	73.0
124.3	.835	13919	1113	32.8	13.92	75.1
136.0	.835	14451	1100	35.6	15.0	77.5

222-110 Volts.

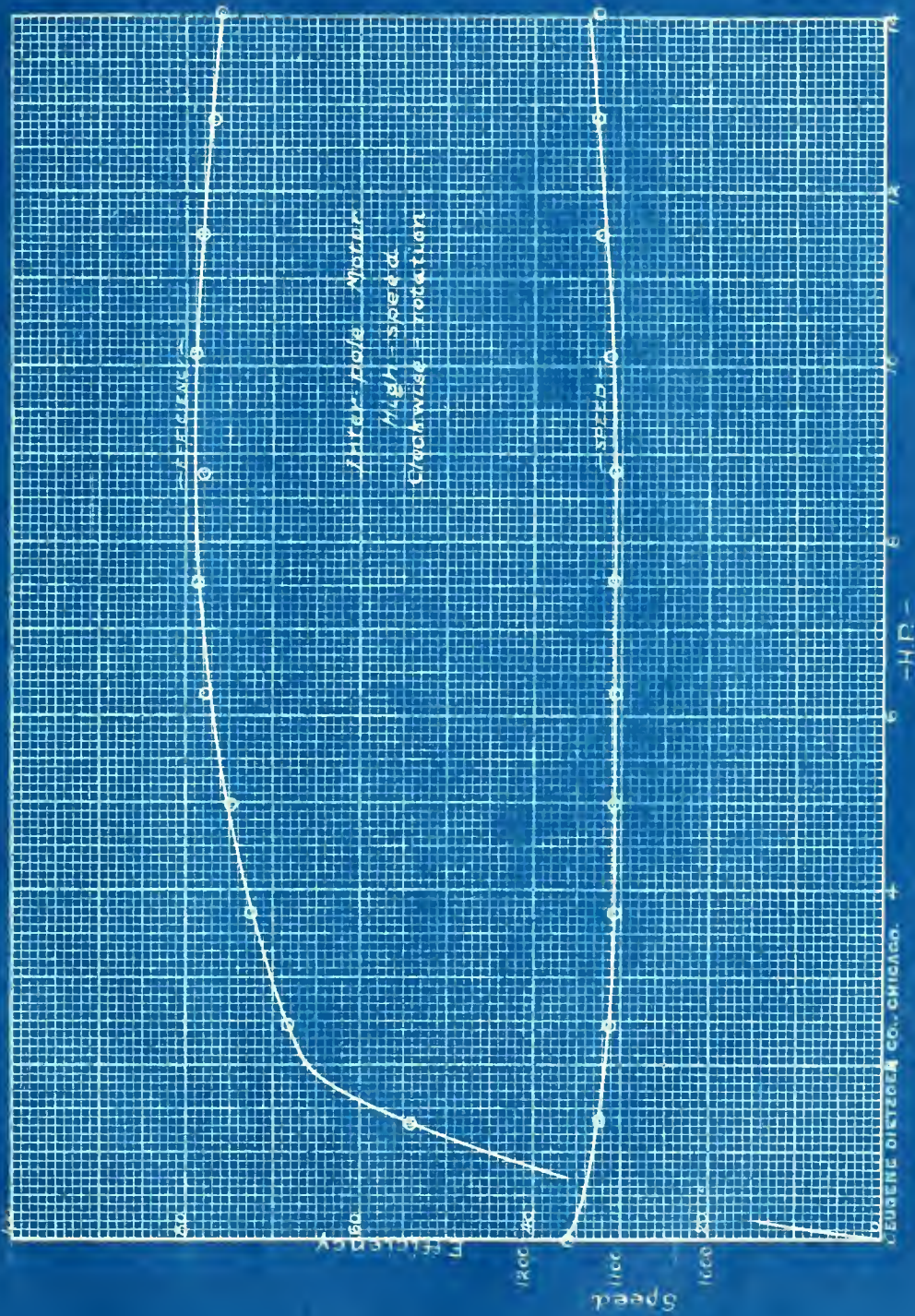












-HP-

EUGENE DISTON CO., CHICAGO.



# Interpole Motor

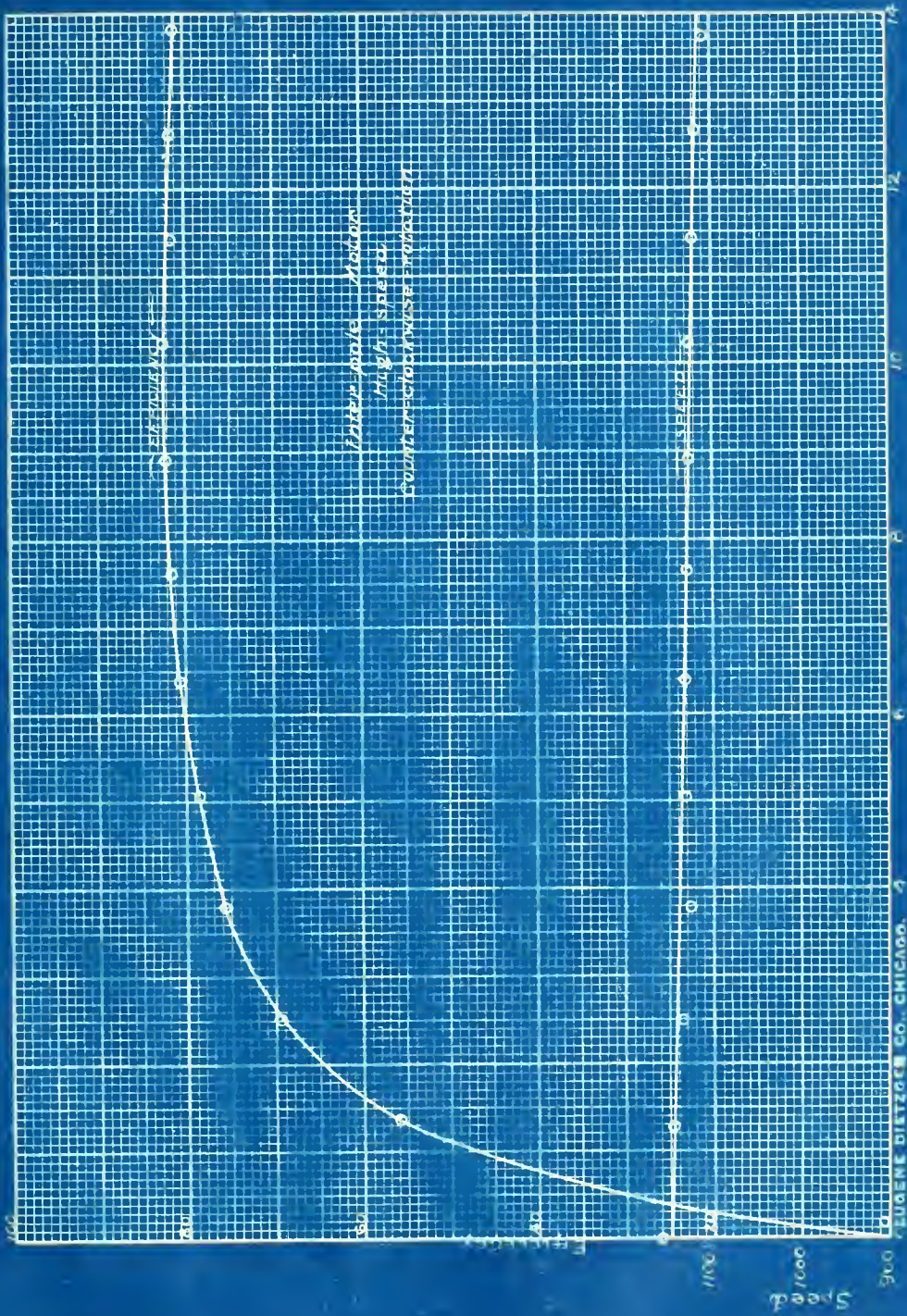
High Speed		Counter Clockwise Rotation.				
la.	I.	<i>Watt</i> Input	Speed	Wt.	H. S.	Eff.
3.2	.805	440	1150	0	0	0
15.7	.805	1015	1142	3.7	1.39	57.2
23.6	.805	2634	1130	5.8	2.49	69.5
33.4	.905	<b>3752</b>	1130	8.8	3.79	75.2
43.0	.905	4818	1128	11.8	5.03	78.7
53.	.805	5918	1128	14.8	6.37	80.4
63.1	.805	7039	1124	17.8	7.64	81.1
73.5	.805	8173	1124	20.8	8.92	81.4
84.3	.805	9361	1124	23.8	10.21	81.5
94.2	.805	10461	1117	26.8	11.41	81.5
104.2	.805	11551	1107	29.3	12.53	81.2
113.4	.805	12562	1089	32.8	13.62	80.3
122.3	.905	13541	1076	35.8	14.70	81.0
132.7	.805	14635	1056	38.8	15.63	79.5

3.2	.8	440	1150	0	0	0
16.1	.8	1059	1148	3.16	1.33	56.
23.6	.8	2684	1133	5.8	2.50	69.6
33.2	.8	3740	1128	8.8	3.78	75.5
43.0	.8	4818	1130	11.8	5.08	78.9
53.1	.8	5929	1130	14.8	6.38	80.3
62.7	.79	6984	1136	17.9	7.64	81.7
72.9	.79	8106	1129	20.8	<b>8.95</b>	82.4
83.8	.79	9305	1126	23.8	10.22	82.1
94.2	.79	10449	1120	26.8	11.42	81.3
104.5	.79	11582	1116	29.8	12.63	81.3
115.0	.79	12737	1104	32.8	13.82	81.0
125.3	.79	13370	1091	35.9	14.9	80.2
134.7	.79	14904	1075	38.8	15.89	79.6

-----110 Volts.





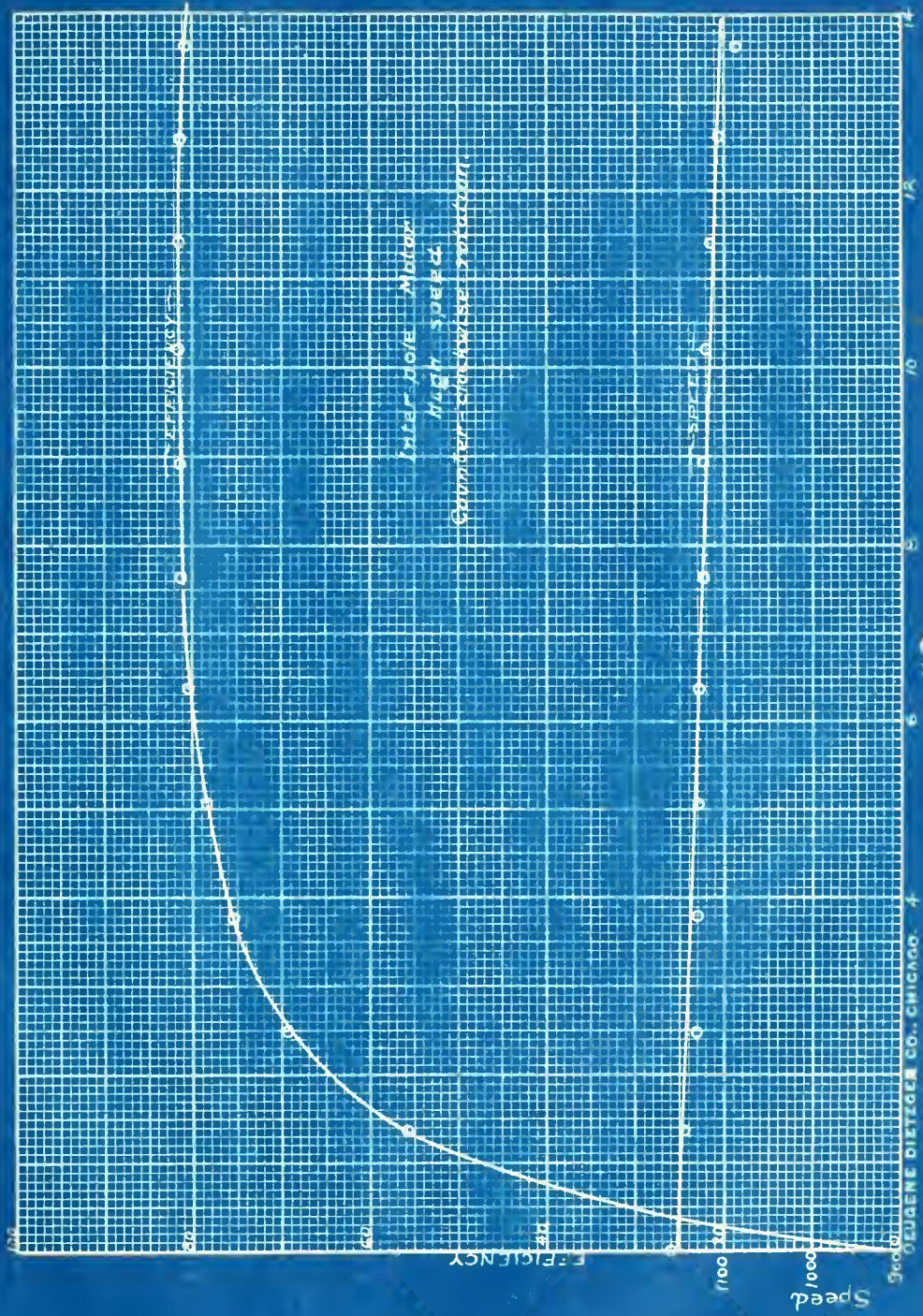


1000 ft/min

EUGENE DIEZEL CO., CHICAGO, ILL.







Speed  
Efficiency  
Inter-Joint Motion  
High Speed  
Gummier's Characteristic Motion  
EUGENE DIETZGEN CO., CHICAGO, ILL.



# Interpolate Motor.

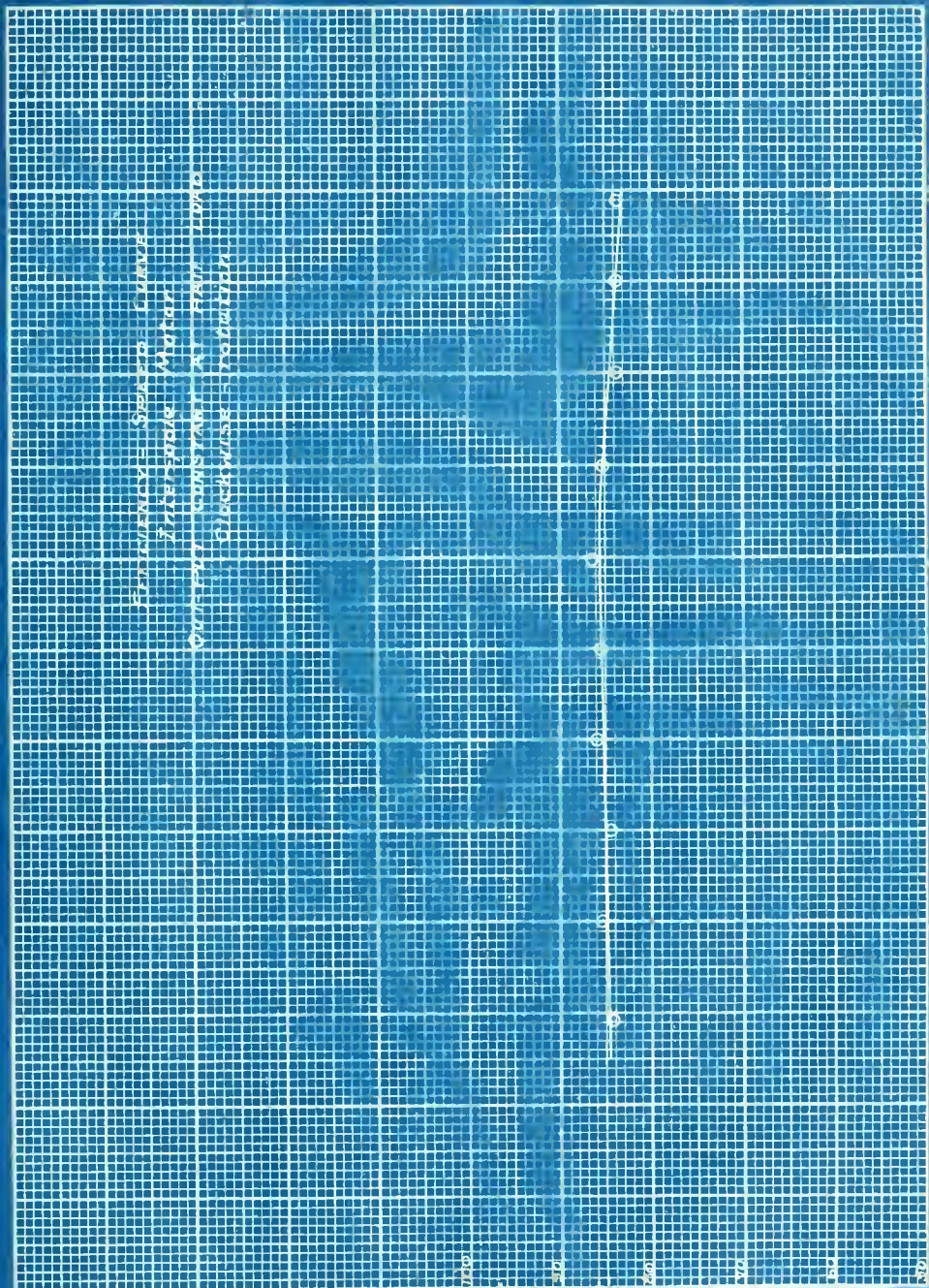
Ia	Half Load (Constant)		Counter	Clockwise Rotation.		
	If.	Watt Input.	Speed.	Wt.	H. P.	Eff.
59.8	4.04	7022	300	47.9	7.62	31.
59.0	2.35	3743	400	42.2	7.5	43.
59.1	1.79	3695	500	39.53	7.5	57.3
59.8	1.55	3743	600	32.8	7.5	67.
59.8	1.27	3717	700	28.14	7.5	75.4
59.8	1.13	3702	800	24.6	7.5	83.5
60.	1.01	3711	900	21.36	7.5	88.68
60.1	.94	3714	1000	19.69	7.5	93.42
62.5	.83	3363	1100	17.9	7.5	96.4
65.6	.77	7086	1130	16.95	7.5	79.

Half Load (Constant)			Clockwise Rotation.			
59.1	4.05	3343	300	47.9	7.34	34.4
57.0	2.41	3535	400	42.2	7.5	35.7
58.4	1.82	3322	500	39.53	7.5	34.5
57.7	1.5	3512	600	32.8	7.5	33.2
53.0	1.38	3520	700	28.14	7.5	35.3
57.7	1.13	3471	800	24.6	7.5	33.5
53.7	1.02	3539	900	21.36	7.5	35.2
59.8	.83	3680	1000	19.69	7.5	37.3
59.8	.94	3670	1100	17.9	7.5	32.7
60.0	.8	3338	1130	16.95	7.5	35.7

E-- 110 Volts.







Efficiency (%) vs. Speed (ft/sec)  
The curve shows that efficiency increases with speed, but at a decreasing rate. The curve is labeled 'Efficiency (%)' and 'Speed (ft/sec)'.

EUGENE DIEZEL CO., CHICAGO, ILL.





Efficiency - Speed Curve

Inter-pole Motor

Current constant at 17.5 amp

Counter clockwise rotation

Efficiency

100

90

80

70

60

50

EUGENE DISTRICT CO. CHICAGO

400

600

800

1000

1200

1400

1600

1800

2000

2200

2400

2600

2800

3000

3200

3400

3600

3800

4000

4200

4400

4600

4800

5000

5200

5400

5600

5800

6000

6200

6400

6600

6800

7000

7200

7400

7600

7800

8000

8200

8400

8600

8800

9000

9200

9400

9600

9800

10000

10200

10400

10600

10800

11000

11200

11400

11600

11800

12000

12200

12400

12600

12800

13000

13200

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61000

61200

61400

61600

61800

62000

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63400

63600

63800

64000

64200

64400

64600

64800

65000



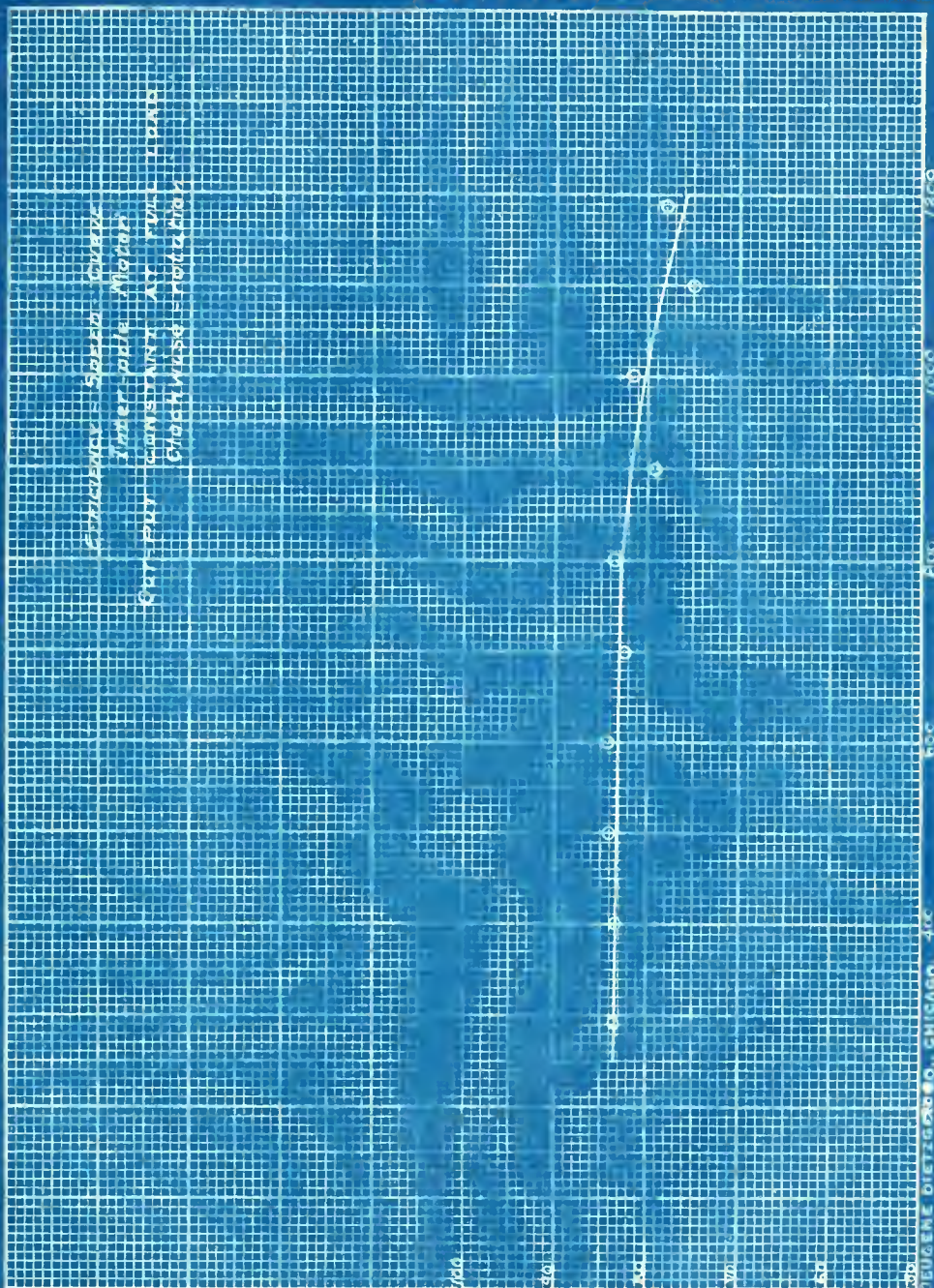
# Interpole Motor

Full Load (Constant)			Clockwise Rotation.			
Ia	<del>1 f</del>	<sup>Watt</sup> Input	Speed	W. T	H. P.	EFF.
121.3	3.9	13837	292	135.6	15	31.5
120	2.40	13474	400	98.5		8.32
119	1.9	13299	500	78.73		84.25
119	1.57	13256	600	65.66		84.5
131.8	1.35	13546	700	56.26		82.6
120.3	1.20	13440	800	49.23		83.3
127.3	1.03	14171	900	43.74		79.1
123.6	.94	13669	1000	39.33		81.0
127.1	.85	14916	1100	35.74		75.
129.5	.8	14333	1190	33.08		78.

Full Load (Constant)			C. C. Rotation.			
119.	3.06	13525	292	135.6	15	32.3
117.	2.45	13139	400	98.5		35.2
119	1.88	13296	500	78.73		84.25
120	1.5	14701	600	65.66		73.2
120.8	1.3	13431	700	56.26		83.3
122.3	1.13	13577	800	49.23		82.5
120.8	1.0	13398	900	43.74		83.6
126.8	.87	14043	1000	39.33		79.8
127.	.8	14058	1100	35.74		79.75
127.8	.74	14159	1190	33.08		79.2



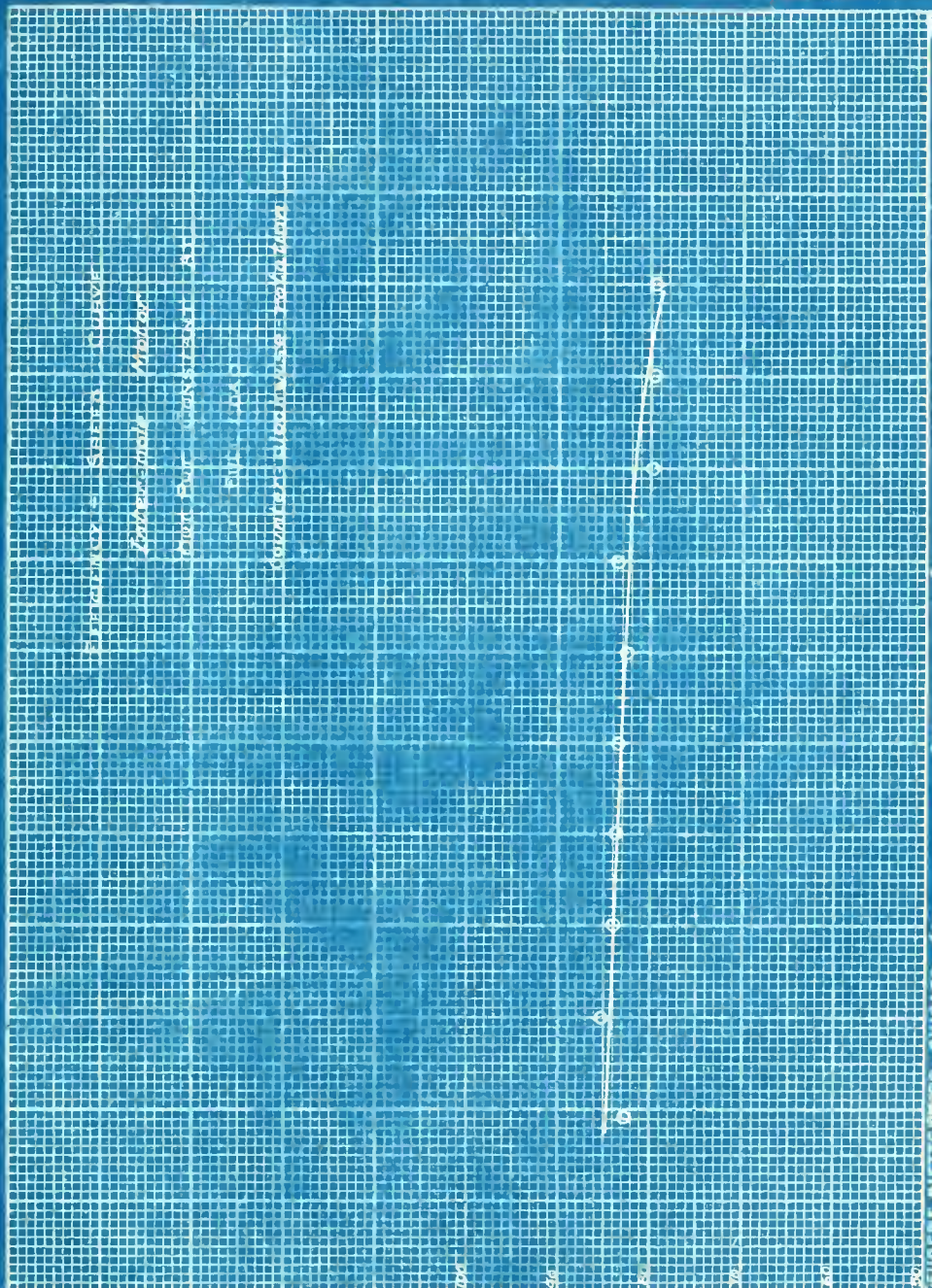




Speed of Sound







STUDENT DISTANCE-SPEED-CHART-1000



# Lincoln Motor

Low Speed

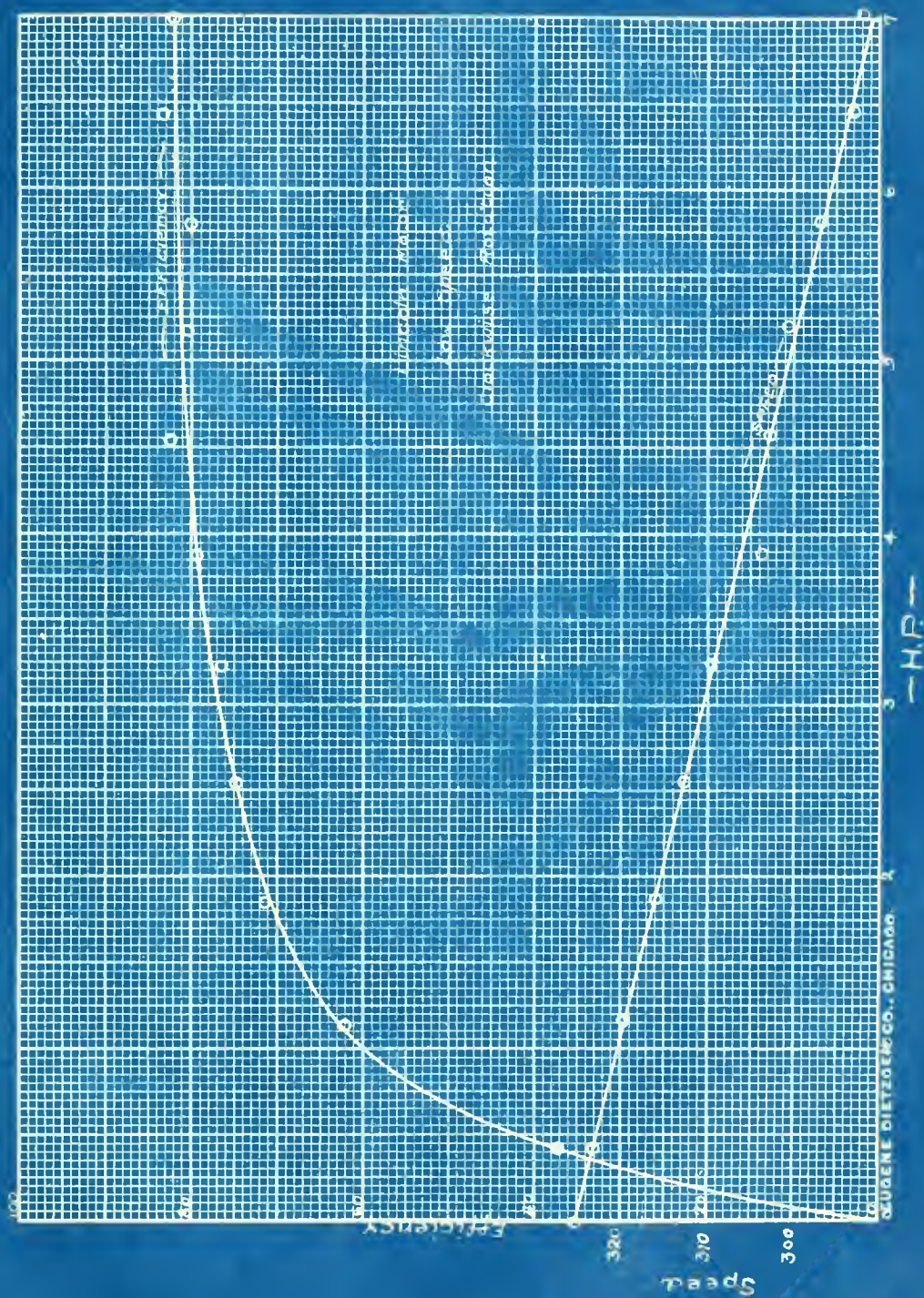
Clockwise Rotation.

1a.	1f.	Watt input	Speed	Wt.	H.P.	Eff.
2.5	2.33	533	325	0.	0.	6.
5.3	2.33	542	322	3.5	1.430	33.
10.3	2.35	1391	320	9.5	1.16	32.
15.7	2.35	1985	313	15.5	1.87	70.4
21.4	2.35	2312	312	21.5	2.53	71.2
26.4	2.35	2132	308	27.5	3.24	73.4
30.3	2.35	3343	305	33.5	5.2	74.3
36.4	2.35	4232	303	39.5	4.75	30.2
44.4	2.35	4912	301	45.5	5.31	30.7
46.7	2.32	5392	303	51.5	5.75	72.3
48.2	2.32	5323	303	57.5	6.42	75.2
55.0	2.32	61.05	293	63.5	7.10	34.
61.0	2.32	6965	2.93	69.5	7.77	34.6
5.5	2.35	365	325	3.5	1.036	7.7
10.5	2.35	1423	320	9.5	1.17	31.2
15.6	2.32	1917	313	15.5	1.28	72.3
20.7	2.32	2532	314	21.5	2.52	76.4
26.5	2.32	3170	312	27.5	3.25	76.5
31.2	2.32	3687	304	33.5	5.2	72.1
36.1	2.32	4225	303	39.5	4.75	30.7
41.9	2.31	4832	301	45.5	5.23	30.1
47.6	2.31	5490	301	51.5	5.31	30.4
51.3	2.30	5920	293	57.5	6.51	30.2
57.5	2.30	6579	293	63.5	7.03	30.2
62.1	2.29	7093	291	69.5	7.72	31.4

110 Volts.









# Line in test.

Low Speed

Counter Clockwise Rotation.

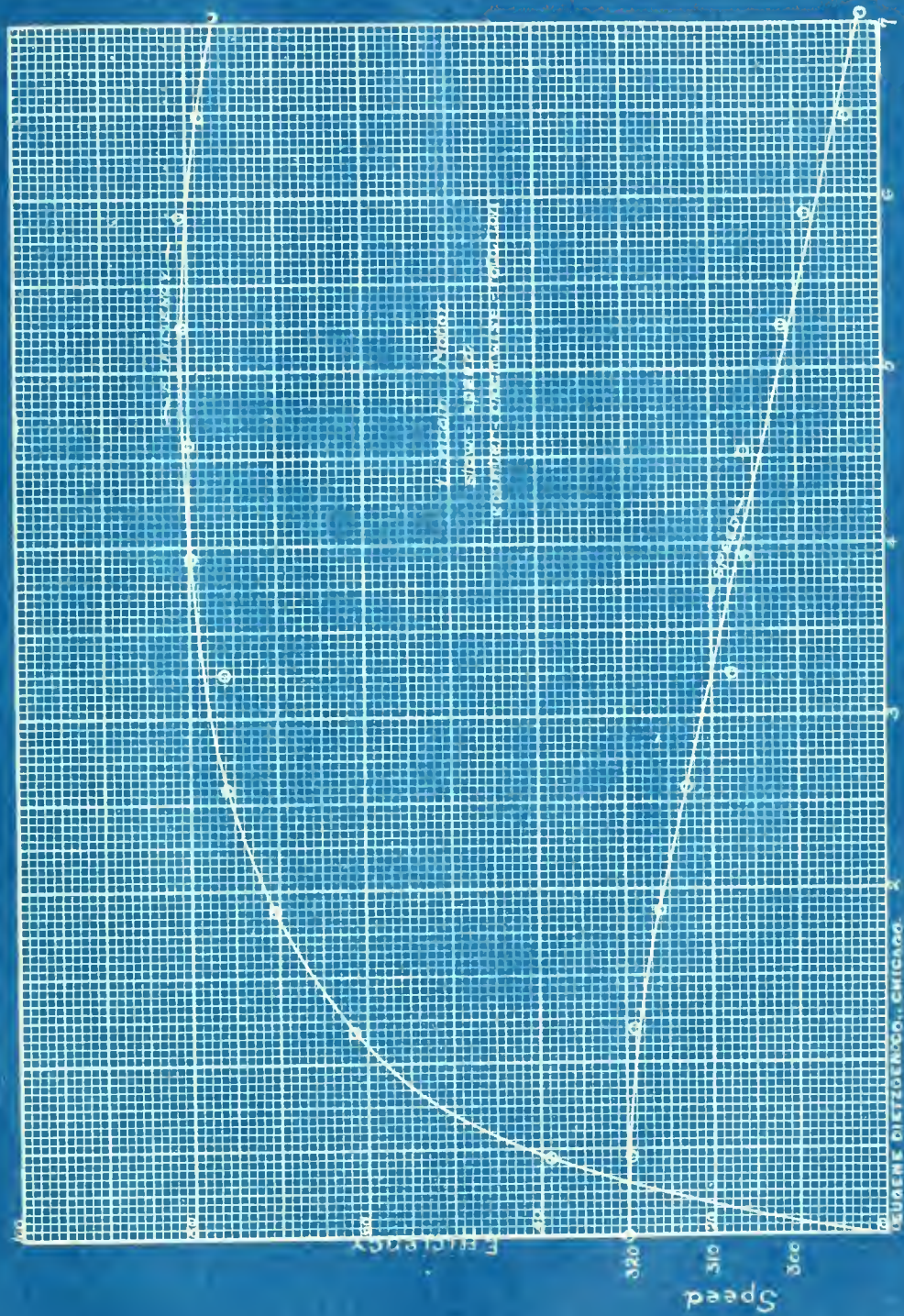
1a.	1f.	Ratio Input	Speed.	t.	K. D.	WTR.
3.6	2.5	371	500	0.	0.	30.
5.5	2.43	373	510	5.7	1.45	30.7
10.75	2.43	1440	510	0.7	1.16	30.0
15.6	2.43	1002	513	15.7	1.0	70.3
20.9	2.42	25.65	513	21.7	2.3	73.0
26.3	2.42	3159	506	27.7	3.37	76.4
31.0	2.42	5676	504	35.7	3.9	78.7
33.5	2.42	4381	502	39.7	4.52	79.4
41.5	2.42	4751	501	45.1	5.24	80.0
46.0	2.41	5635	500	51.7	5.89	80.0
54.2	2.41	6237	503	57.7	6.44	79.4
61.8	2.40	7037	501	63.7	7.06	78.3

5.5	2.4	369	500	5.7	1.450	30.7
10.5	2.39	1417	510	0.7	1.16	30.0
15.6	2.38	1077	513	15.7	1.07	70.3
20.7	2.38	2538	514	21.7	2.33	73.0
26.7	2.37	3107	510	27.7	3.37	76.4
31.2	2.37	5602	508	35.7	3.93	78.4
37.0	2.37	4330	503	39.7	4.35	80.0
41.0	2.36	4338	500	45.7	5.26	80.7
46.0	2.36	5580	500	51.7	5.89	79.4
53.0	2.35	6088	505	57.7	6.40	79.0
59.0	2.35	6748	503	63.7	7.11	78.7

2--110 Volts.







-H.P.-

EUGENE DIETZGEN CO., CHICAGO





# High Speed Motor.

High Speed Motor. (110 Volts.)

Ta.	Tf.	Speed.	Rt.	H.P. at 110 Volts.		
				Mat.	HLF.	Eff.
2.	2.31	365	1.	474	0.	0.
3.3	2.31	451	1.7	1137	0.53	0.4
15.6	2.509	494	4.5	1970	1.7	11.
22.0	2.307	635	7.5	3071	2.45	20.
28.	2.507	678	9.5	3353	2.5	24.
35.4	2.307	805	12.0	4147	4.1	28.5
40.0	2.507	893	14.5	4933	4.94	35.5
42.5	2.38	884	17.0	5373	5.72	37.2
53.0	2.279	875	19.5	6410	6.5	38.5
52.3	2.27	835	22.0	7102	7.25	36.
2.4	2.31	365	1.7	1173	0.53	0.07
13.3	2.3	644	4.5	2043	1.62	10.2
21.4	2.3	865	7.0	3607	2.03	12.0
28.3	2.3	920	9.5	5500	3.33	17.0
54.5	2.3	910	12.0	4042	4.13	22.0
43.0	2.38	900	14.5	4230	4.27	24.4
49.3	2.270	987	17.0	5373	5.75	27.
55.3	2.279	934	19.5	3533	5.57	27.2
22.5	2.27	835	22.0	7124	7.25	25.5

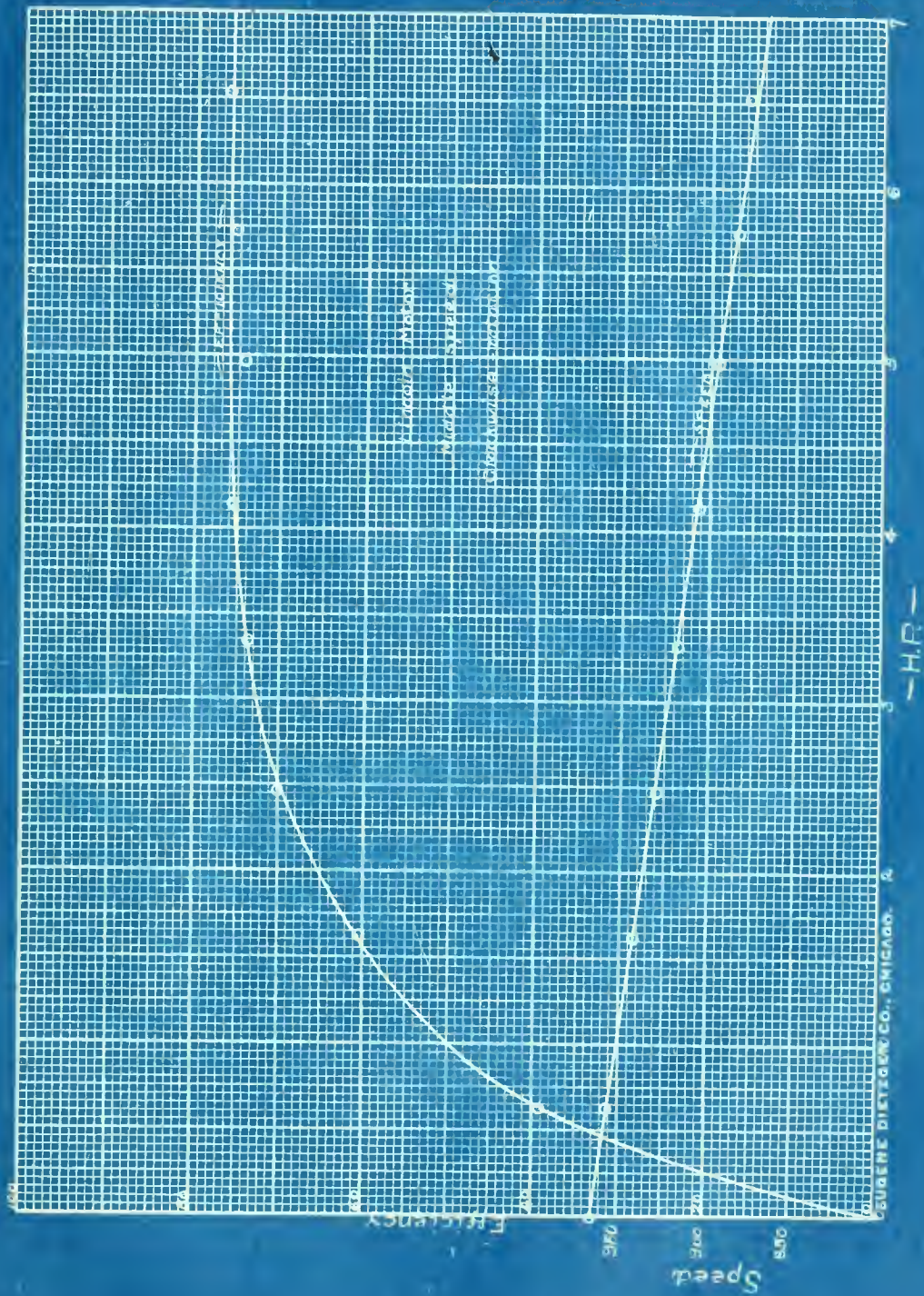
**BARNES-CROSBY COMPANY**

**GENTLEMEN:**

**RESPONDING TO YOURS OF**

**CONCERN**

**CHICAGO**







# Lincoln Motor

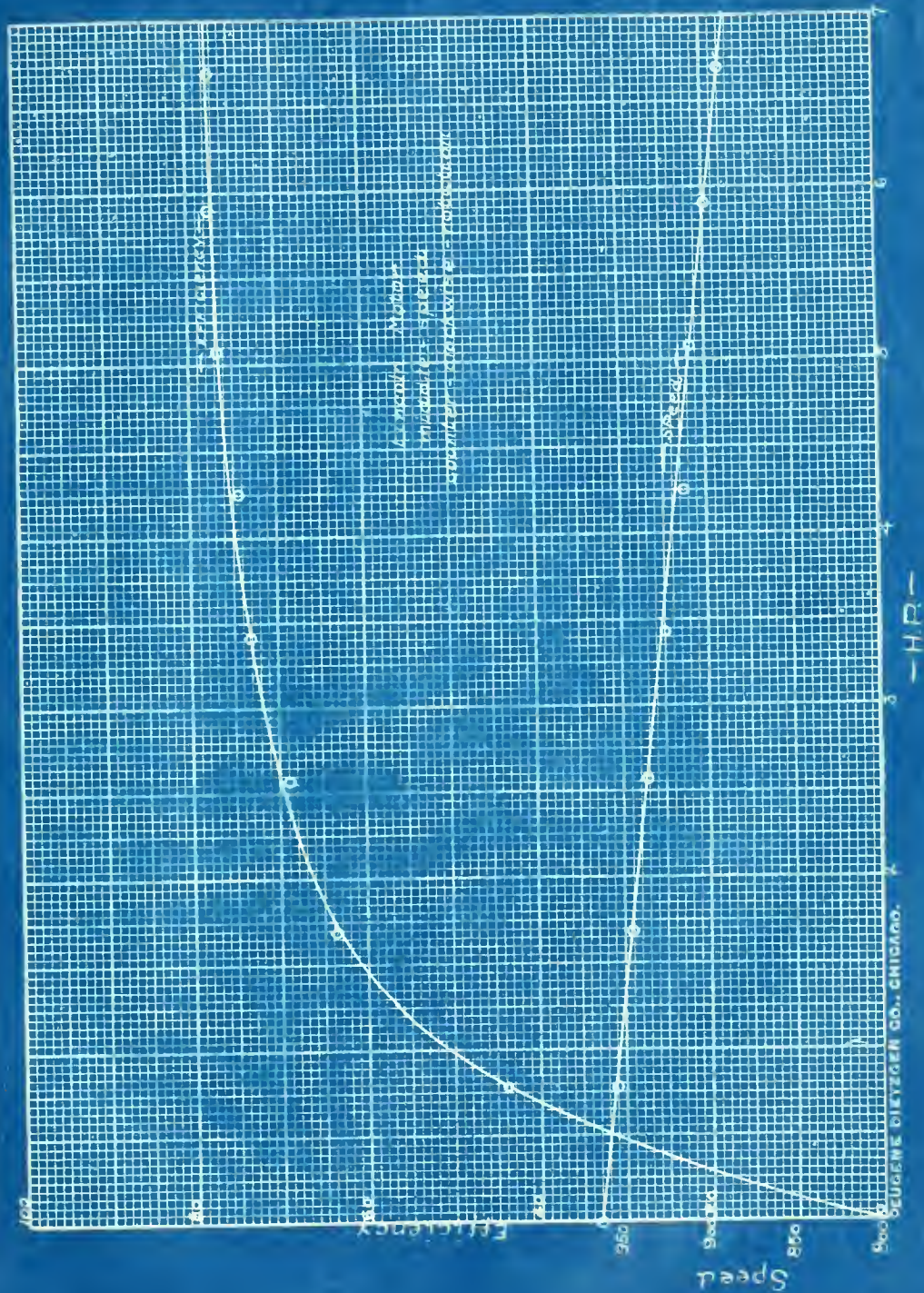
Middle Speed

Counter Clockwise Rotation.

Ia	If	<i>Watt</i> Input	Speed	Weight	H.P.	Eff.
2.05	2.41	490	963	0	0	0
9.9	2.40	1353	953	2.2	.8	44.2
15.6	2.405	1980	945	4.7	1.60	63.6
22.9	2.40	2783	934	7.2	2.56	68.6
29.6	2.39	3519	923	9.7	3.41	72.4
36.5	2.37	4275	911	12.2	4.24	74.0
42.0	2.38	4991	904	14.7	5.06	75.7
49.2	2.37	5672	900	17.2	5.9	77.6
56.7	2.37	6497	892	19.7	6.7	77.0
65.6	2.37	7256	881	22.2	7.45	76.5
9.5	2.4	1309	955	2.1	.765	43.6
15.6	2.38	1977	945	1.7	1.60	33.0
22.9	2.37	1779	936	7.2	2.57	6 9.00
29.1	2.37	3461	926	9.7	3.42	75.8
36.1	2.37	4231	915	12.2	4.25	74.0
42.3	2.37	4913	908	14.7	5.08	77.2
48.8	2.37	5628	900	17.2	5.9	78.2
56.4	2.37	6464	892	19.7	6.7	77.4
64.0	2.36	7200	881	22.2	7.45	73.2

220- 110 Volts.





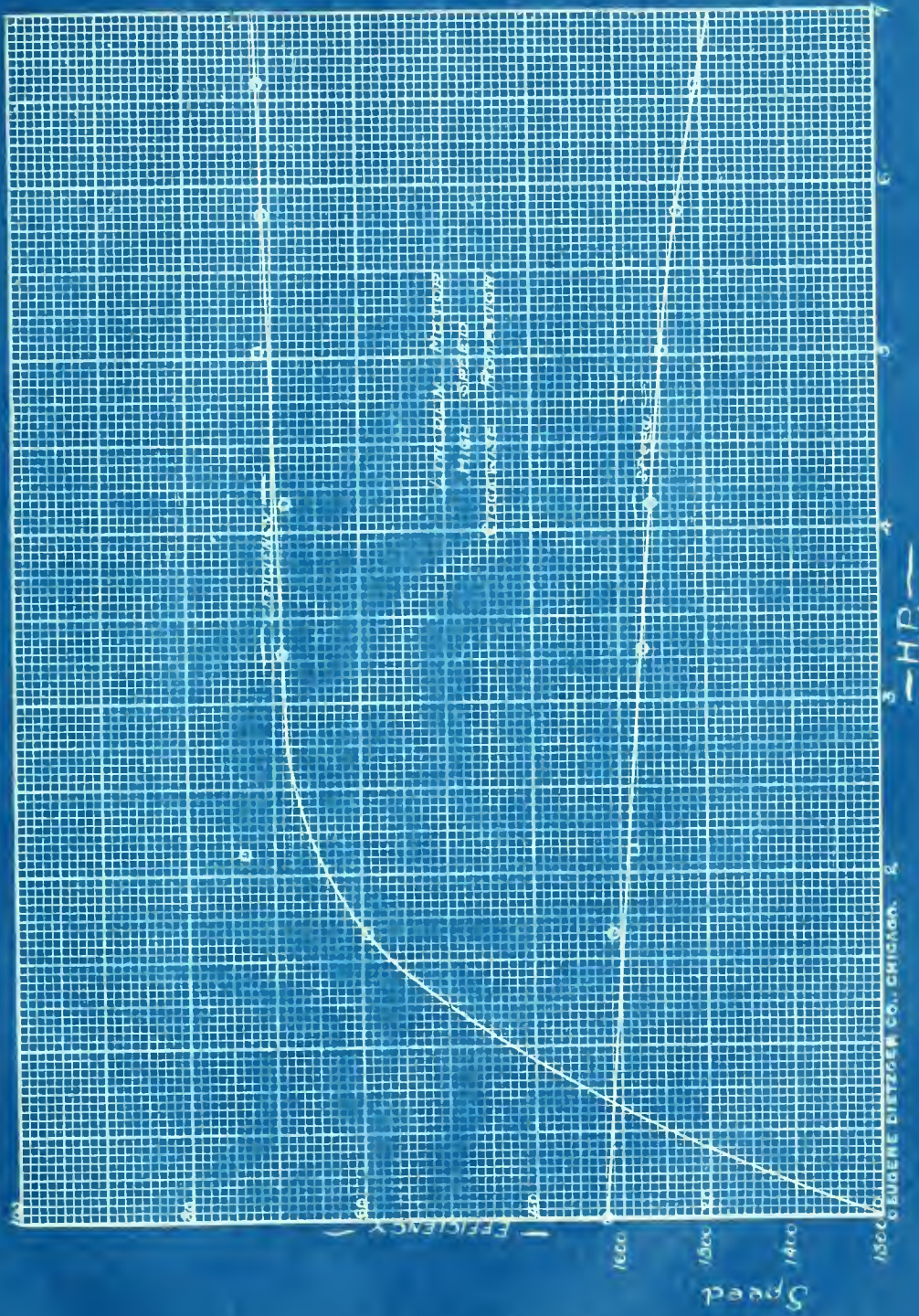




In.	High Speed, Lincoln Motor.		Speed	Blow Pipe Rotation.		
	1 <sup>st</sup>	<i>Heat Input</i>		Wt.	H. P.	Eff.
5.3	2.43	3.63	1330	0	0	0
17.2	2.43	3159	1580	2.5	2.11	73.
30.6	2.42	3632	1560	5.5	3.27	67.2
40.	2.42	4663	1548	7.0	4.13	63.2
45.9	2.41	5314	1540	8.5	5.0	70.2
52.9	2.40	6035	1517	10.0	5.72	71.0
61.6	2.40	7040	1489	11.5	6.53	69.4
67.5	2.38	7683	1439	13.0	7.33	71.6
16.5	2.40	3079	1610	2.7	1.65	59.5
20.6	2.40	3530	1591	3.5	2.12	62.0.
29.1	2.40	3355	1580	5.5	3.32	75.9
37.8	2.38	4412	1572	7.0	4.2	71.0
44.8	2.38	5182	1530	8.5	5.03	72.9
54.0	2.38	6201	1538	10.0	5.83	70.6
59.7	2.37	6817	1519	11.5	6.66	72.3
69.6	2.33	7915	1511	13.0	7.49	70.6

1--110 Volts.









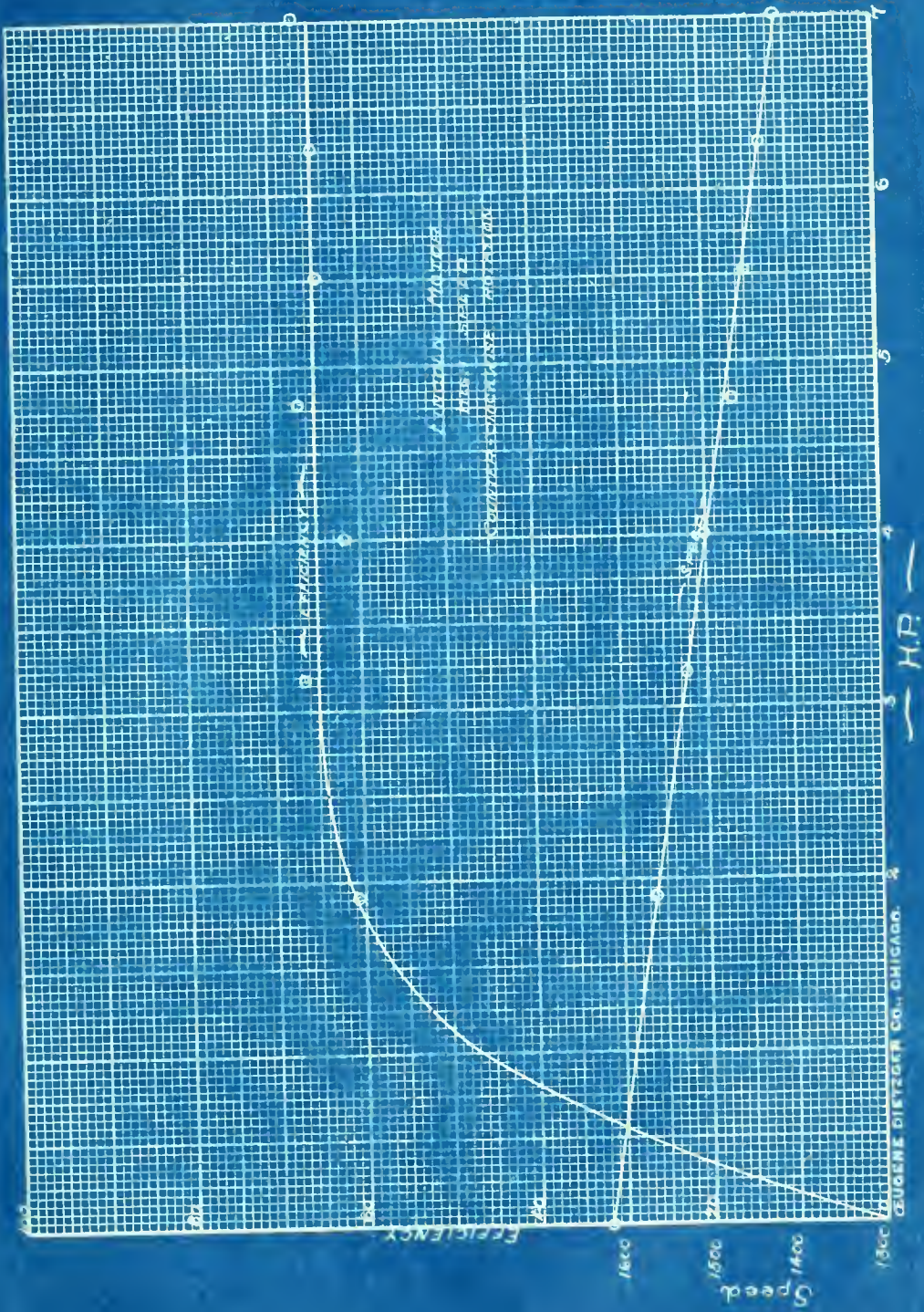
# Lincoln Motor

High Speed		<i>Natt</i>	Counter Clockwise Rotation,			
Ia	If	Input	Speed	Wt.	H P.	Eff
3.7	2.42	373	1620	0	0	0
18.0	2.40	2244	1580	3.0	1.8	30.
30.6	2.39	3323	1523	5.5	3.2	37.0
37.4	2.38	4375	1497	7.0	3.90	38.8
43.8	2.38	5079	1473	8.5	4.73	40.0
54.4	2.38	6245	1430	10.0	5.45	35.0
39.7	2.35	6935	1400	11.5	6.14	36.1
37.5	2.35	7633	1380	13.0	6.85	36.5
3.9	2.38	690	1320	0	0	0
20.2	2.35	2480	1548	3.5	2.03	31.3
30.0	2.35	3553	1520	5.5	3.19	37.0
43.0	2.35	4938	1503	7.0	4.01	30.0
48.0	2.35	5326	1489	8.5	4.32	34.0
56.7	2.35	6495	1470	10.0	5.60	34.4
35.6	2.35	7474	1432	11.5	6.41	34.0
39.6	2.35	7914	1418	13.0	7.18	37.6

2--110 Volts

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# Lincoln Motor

Ia	Half Load (Constant)		Clockwise Rotations.			
	If	<del>Half</del> Input	Speed	Wt.	HP.	Eff
19.9	2.4	2453	500	20.5	2.5	73.1
<b>19.0</b>	<b>2.4</b>	<b>2354</b>	<b>500</b>	13.12	2.5	70.3
20.0	2.4	2464	700	9.38	2.5	75.7
20.4	2.38	2505	900	7.3	2.5	74.5
20.9	2.39	2560	1100	5.96	2.5	73.0
21.0	2.41	2575	1300	<b>5.05</b>	2.5	72.5
23.2	2.41	2817	1450	4.52	2.52	66.4
23.2	2.41	2707	1320	4.05	2.52	69.0

Half Load (Constant)			Counter Clockwise Rotations			
20.6	<b>2.41</b>	2531	320	20.5	2.5	75.3
20.4	2.41	2509	500	13.12	2.5	74.5
21.1	2.40	2585	700	9.38	2.5	72.2
22.0	2.37	2680	900	7.3	2.5	69.7
23.7	2.37	2867	1100	5.96	2.5	65.1
24.0	2.37	2900	1300	<b>5.05</b>	2.5	64.4
23.0	2.40	2893	1450	4.52	2.5	64.3

110-110 Volts.

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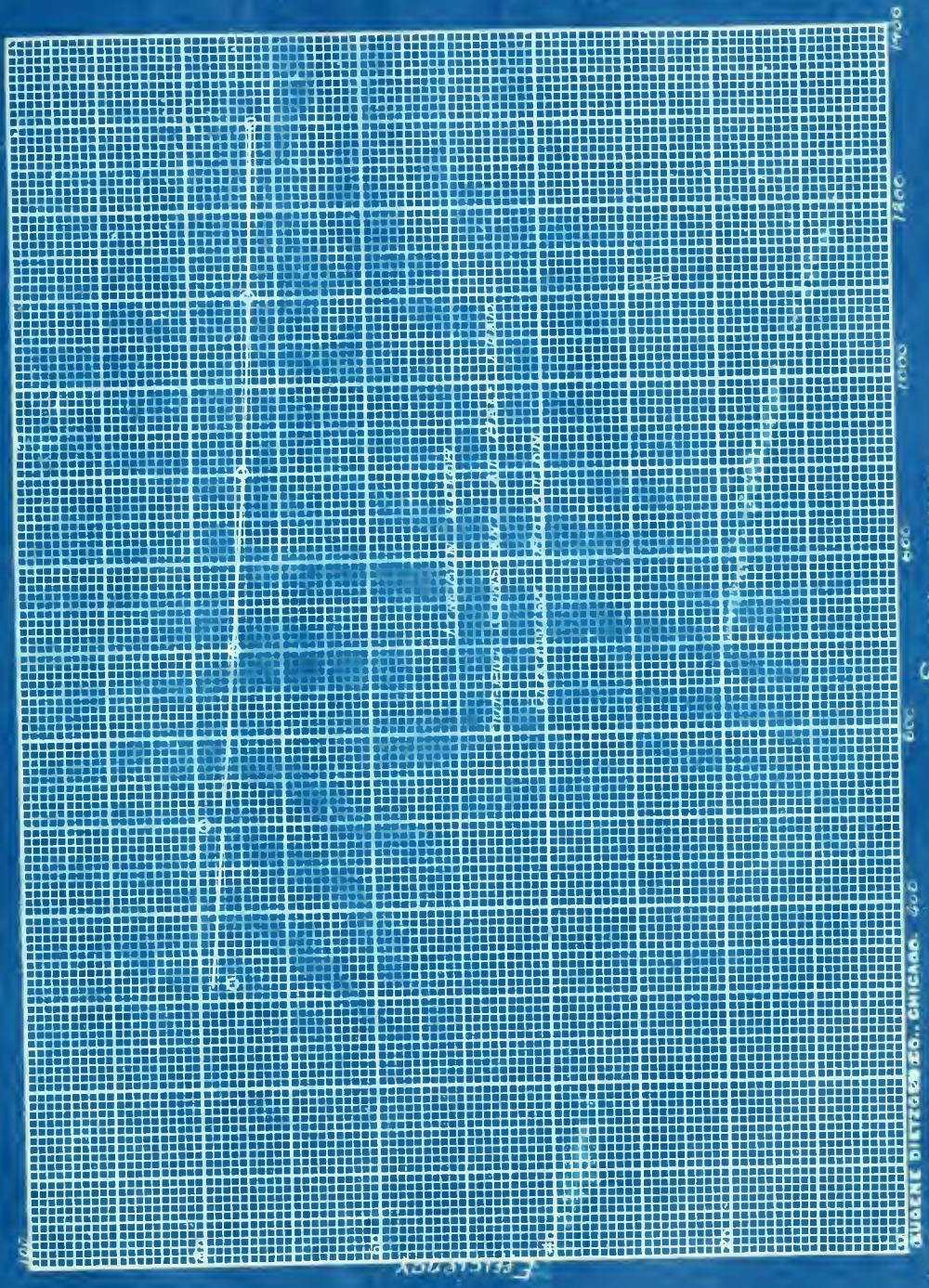
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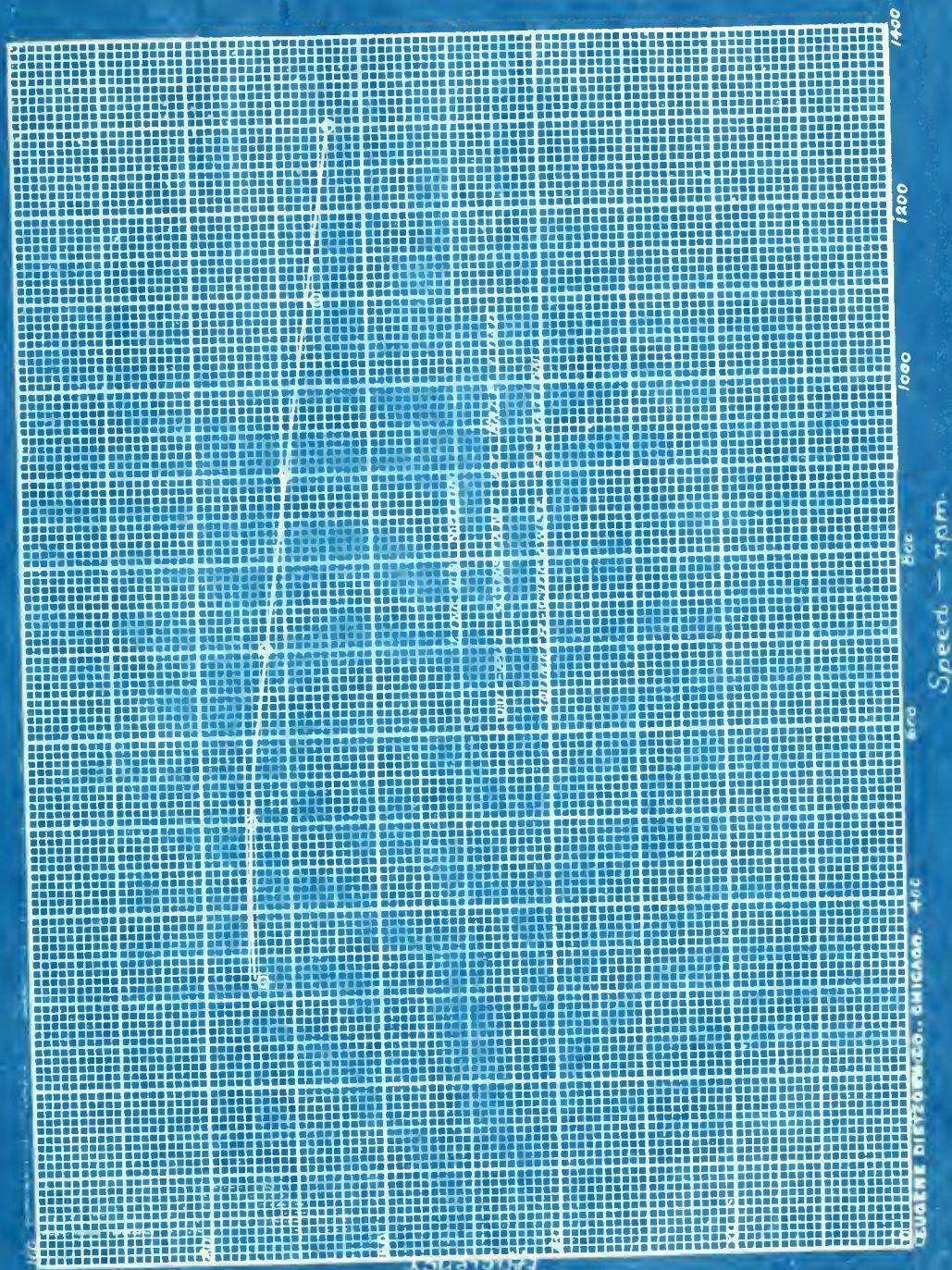
Speed - r.p.m.

Efficiency

STUDENE DIVISION CO., CHICAGO, ILL.









# Lincoln Motor

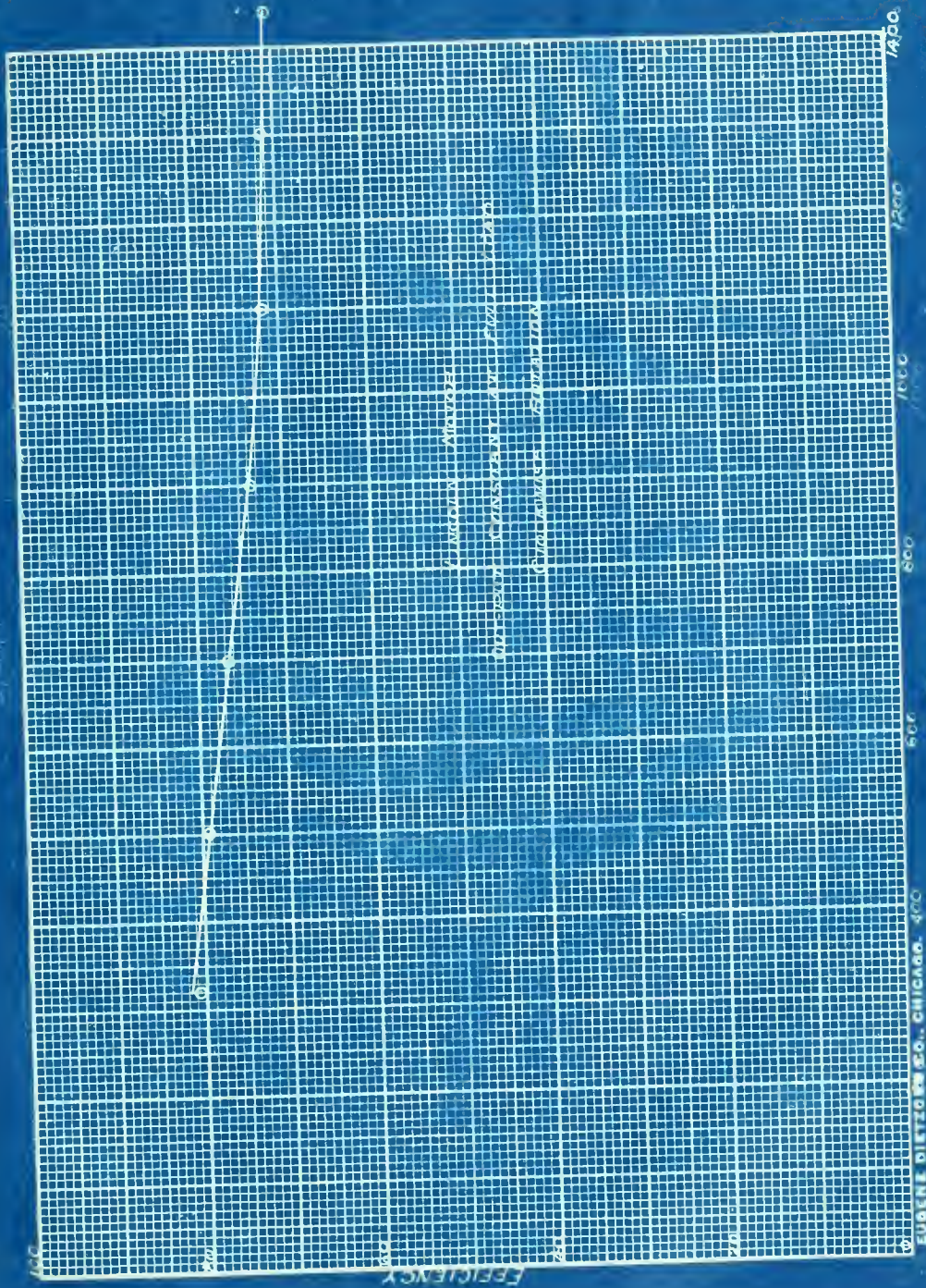
Full Load (Constant)			Clockwise Rotation.			
Ia	If	<sup>Watt</sup> Input	Speed	Wt.	H.P.	Eff.
38.2	2.33	4433	320	41.0	5.0	83.5
40.0	2.37	4660	500	26.25	5.0	81.8
36.7	2.38	4293	700	18.76	5.0	86.9
41.1	2.37	4781	900	14.6	5.0	79.0
43.6	2.37	5056	1100	11.92	5.0	73.7
41.0	2.40	4774	1300	10.1	5.0	78.1
41.5	2.38	4826	1450	9.05	5.0	77.4

Full Load (Constant)			Counter Clockwise Rotation.			
39.6	2.42	4632	320	41.0	5.0	80.7
40.2	2.40	4386	500	26.25	5.0	79.7
41.9	2.40	4873	700	18.76	5.0	73.5
43.8	2.40	5082	900	14.6	5.0	73.5
44.8	2.40	5192	1100	11.92	5.0	71.0
44.8	2.40	5192	1300	10.1	5.0	71.9
45.8	2.40	5302	1450	9.05	5.0	70.4

E--110 Volts.

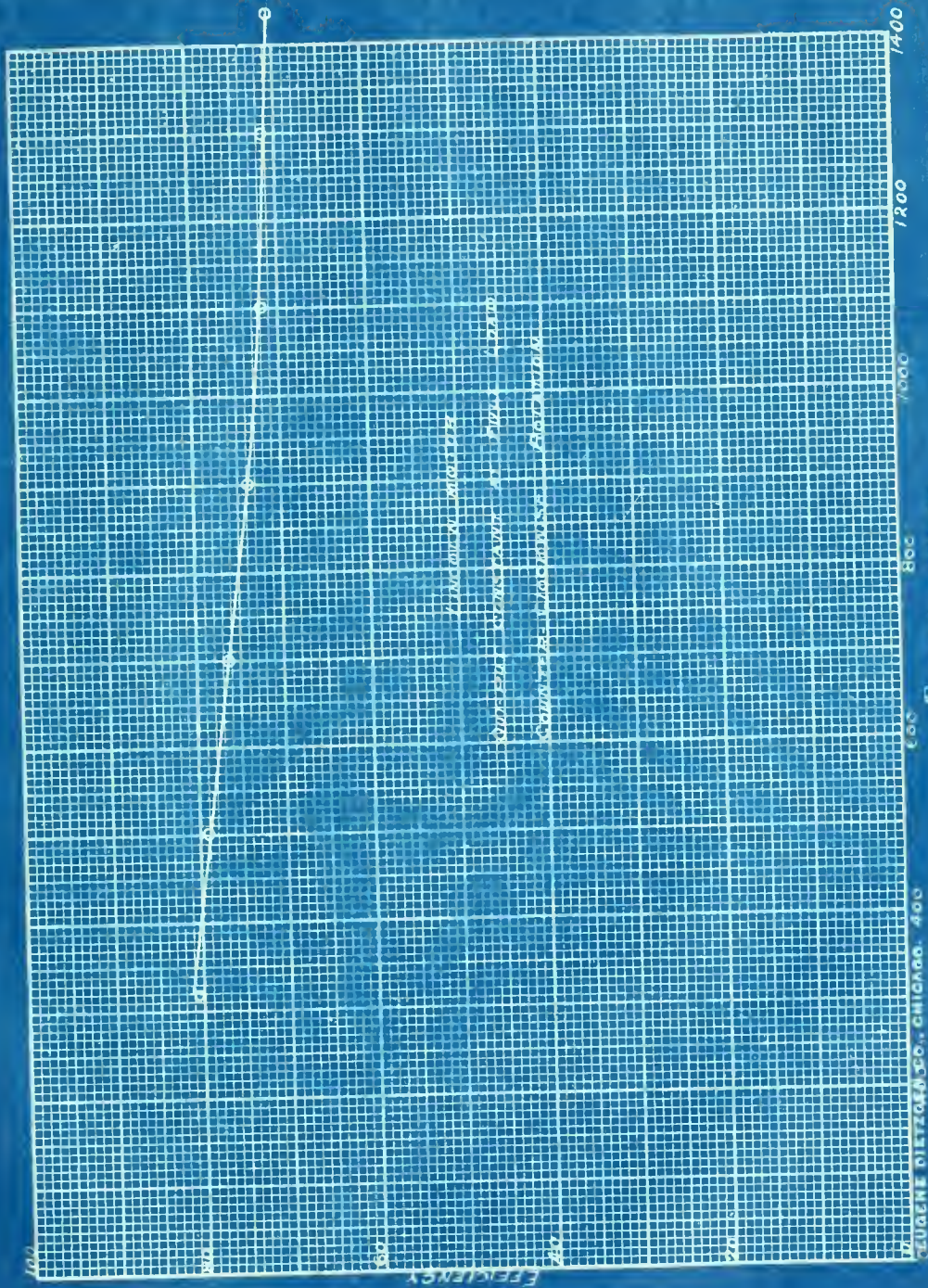












Speed - r.p.m.

EUGENE DETZGER CO., CHICAGO. 400



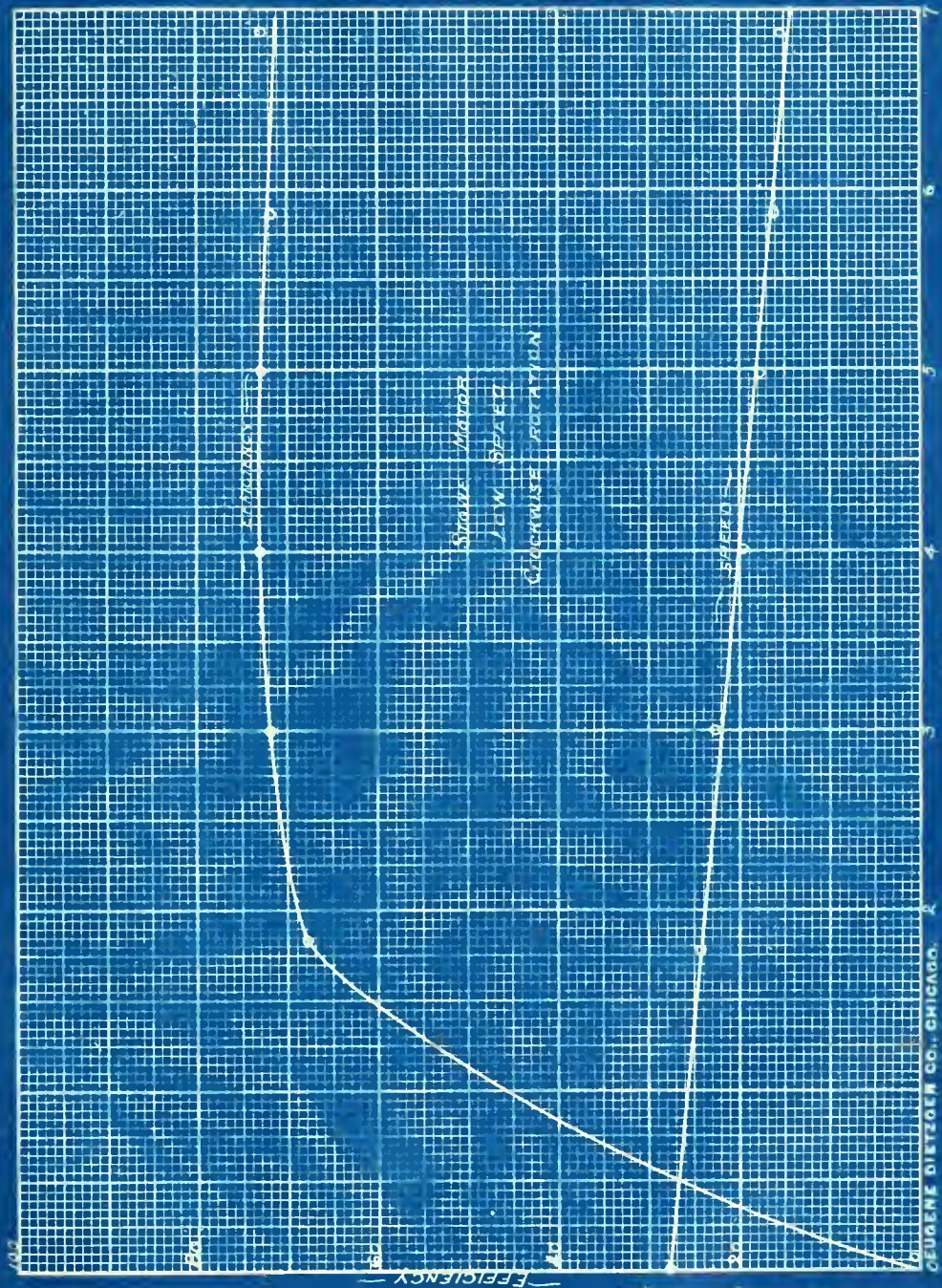


# Stowe Motor

Ia.	If.	Low Speed	Clockwise Rotation.			
		Watt Input	Speed	Wt.	H. P.	Eff.
2.7	1.54	444	380	0.	0.	0.
8.7	1.53	1103	432	2.67	.67	15.1
17.4	1.53	2060	456	7.5	1.27	37.3
26.2	1.53	3028	472	12.5	2.31	51.2
34.8	1.31	5972	523	17.5	3.97	74.3
43.9	1.31	<b>4973</b>	577	22.5	4.91	71.7
53.5	1.31	6007	531	27.5	5.27	72.9
63.1	1.31	7085	549	32.5	6.20	71.5
72.7	1.31	8141	557	37.5	7.33	74.7
7.0	1.31	914	362	1.3	.33	2.36
16.7	1.31	1981	352	7.5	1.20	62.
27.6	1.31	3134	326	12.5	2.03	70.
37.1	1.31	4225	602	17.5	4.01	71.2
45.3	1.31	5132	585	22.5	5.01	72.2
55.3	1.31	6227	561	27.5	5.85	71.3
62.6	1.31	7030	561	32.5	6.25	71.
72.4	1.31	8108	549	37.5	7.34	71.5

E-- 110 volts.





EUGENE DIETZGEN CO., CHICAGO.

HP

Speed





# Stowe Motor

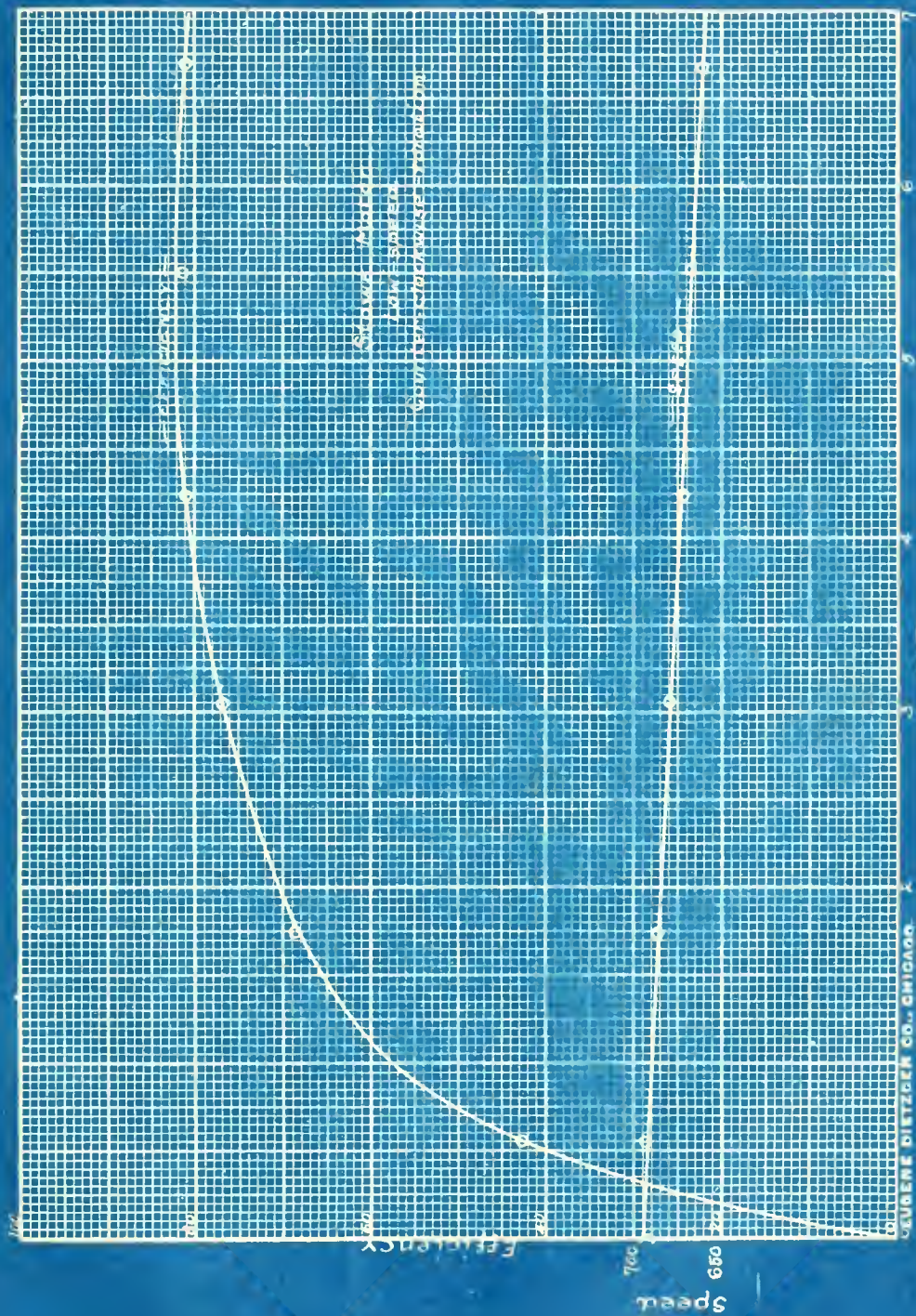
## Low Speed

## Counter Clockwise Rotation.

Ia.	If.	Watt Input	Speed	Wt.	H.P.	Eff.
2.8	1.45	467	695	0.	0.	0.
7.5	1.45	984	637	2.33	.534	45.3
15.6	1.45	1875	680	6.3	1.71	33.
25.5	1.45	2964	675	11.6	2.92	75.
35.0	1.42	4007	635	13.6	4.2	73.5
45.0	1.45	5107	658	21.6	5.41	72.2
54.0	1.45	6099	658	26.3	6.33	71.3
65.0	1.45	7309	650	31.6	7.32	70.3
76.3	1.45	85.52	645	36.3	8.22	77.3
6.	1.45	819	699	1.3	4.023	53.9
15.5	1.45	1864	686	3.6	1.725	69.2
24.7	1.45	2876	680	11.6	3.0	77.5
34.	1.45	3899	675	13.6	4.27	71.2
44.3	1.42	5662	639	21.6	5.50	67.2
54.9	1.42	61.05	658	26.3	6.36	60.5
68.	1.42	7336	658	31.6	7.32	77.5
75.4	1.42	8450	650	36.3	8.22	82.0
7.5	1.42	981	709	2.2	.59	47.0
16.0	1.42	1916	693	6.3	1.74	67.8
25.	1.42	2906	683	11.6	3.30	77.7
35.0	1.42	3935	680	13.6	4.3	69.3
44.3	1.42	5034	675	21.6	5.55	61.5
53.1	1.41	6326	635	26.3	6.73	70.4
63.8	1.41	7725	650	31.6	7.32	65.7
79.4	1.41	8889	659	36.6	8.20	74.2

110 Volts.





EUGENE PLETZLER CO., CHICAGO.

—HP—



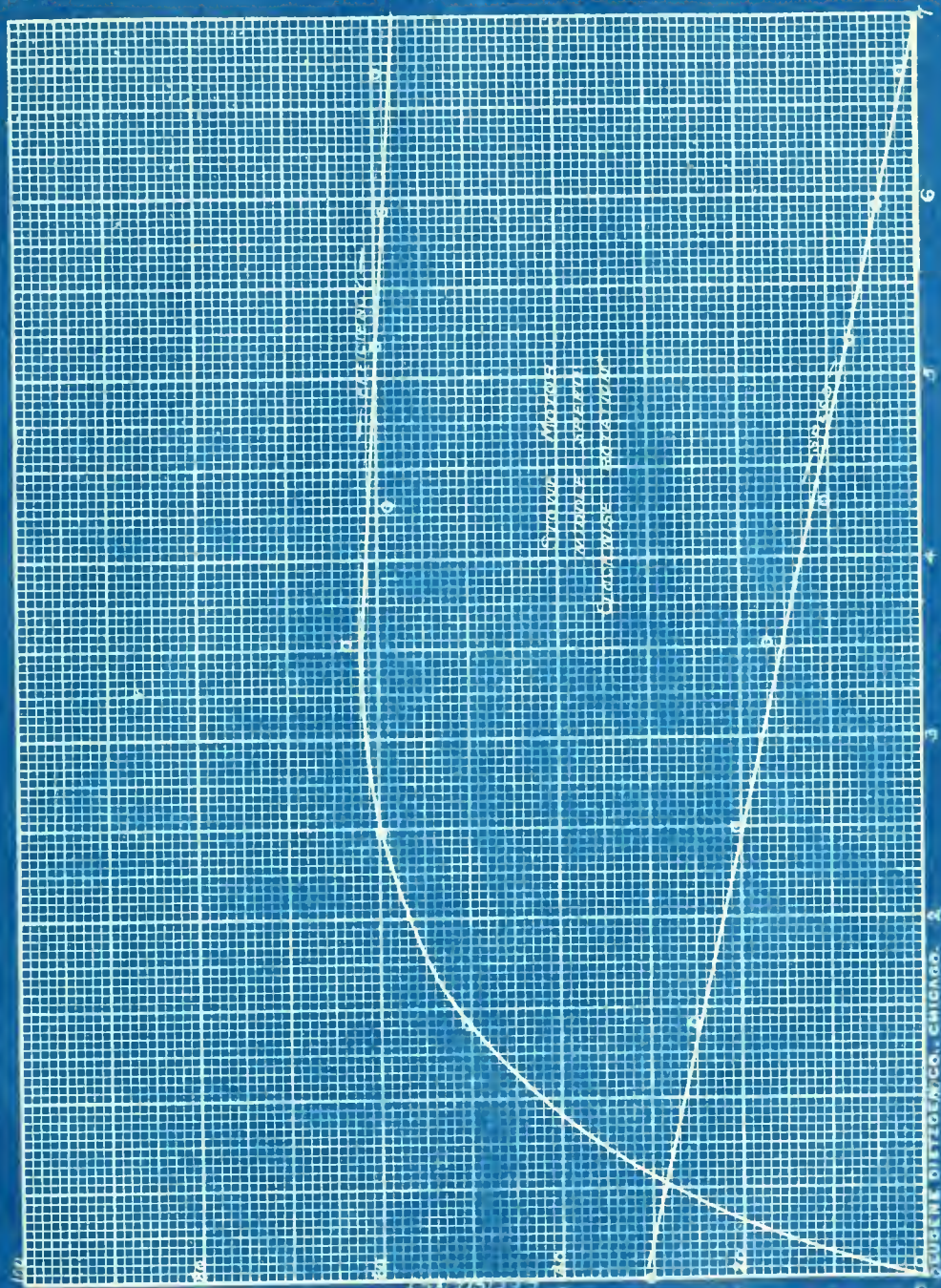


# Stone - 1.

1a.	Middle Speed.		Clockwise Rotation.			
	If	Input	Speed	Wt.	H. S.	1.1.
7.9	1.32	1003	1165	0.	0.	0.
15.9	1.32	1033	1032	1.5	1.31	50.
16.7	1.31	2201	1051	3.5	1.41	57.5
27.6	1.31	3130	1009	6.5	2.40	51.5
37.1	1.51	4225	973	9.5	3.52	32.1
49.8	1.31	5322	395	12.5	4.23	53.5
57.0	1.51	6414	377	15.5	5.18	60.8
66.5	1.31	7359	247	18.5	5.37	62.5
75.0	1.31	8394	813	21.5	6.39	59.5
14.8	1.52	1775	1062	1.7	1.50	22.
16.4	1.32	1949	1051	3.5	1.4	53.7
23.6	1.52	3071	1002	6.5	2.48	60.5
35.7	1.32	4072	937	9.5	3.5	64.2
46.8	1.31	5292	913	12.5	4.35	61.8
57.3	1.31	6447	371	15.5	5.15	59.7
68.0	1.31	7624	835	18.5	5.32	57.5
74.4	1.31	8328	316	21.5	6.32	55.8

E-- 110 Volts.





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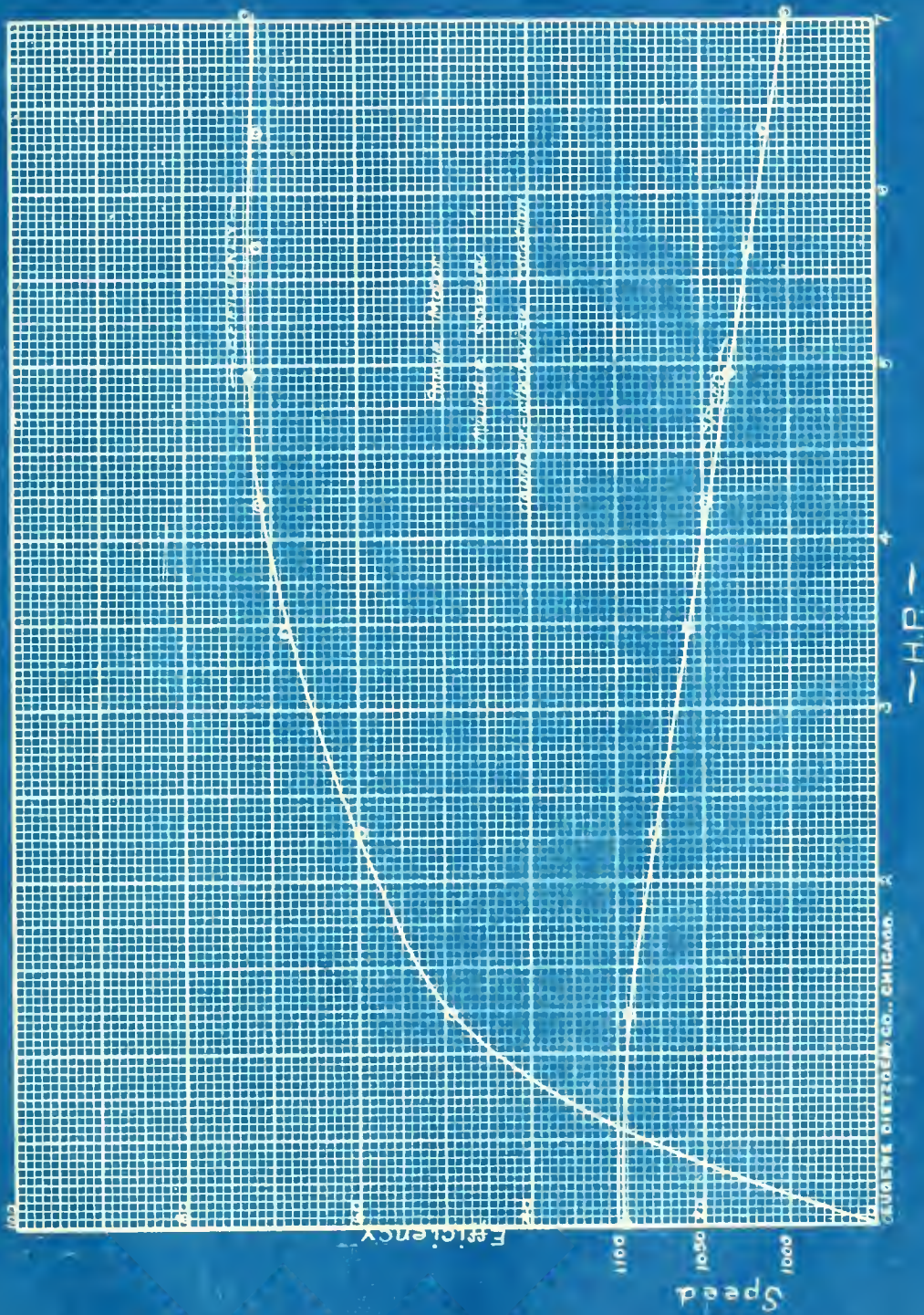




# Stowe Motor

Middle Speed		Counter Clockwise Rotation.				
Ia	If.	<i>Ha</i> tt Input	Speed	Wt.	H. P.	Eff.
5.7	1.45	786	1095	0	0	0
15.5	1.45	1864	1095	3.0	1.33	52.
24.7	1.42	1873	1089	5.6	2.32	59.5
33.6	1.41	3851	1070	8.6	3.5	67.2
39.3	1.41	4478	1062	10.6	4.28	71.5
45.8	1.41	5193	1050	12.6	5.04	72.6
54.4	1.41	6139	1042	14.6	5.8	70.5
60.0	1.41	6755	1030	16.6	6.51	72.0
65.7	1.41	7332	1018	18.6	7.22	73.05
81.2	1.41	9087	970	22.6	8.55	63.7
6.6	1.41	881	1095	0	0	0
16.6	1.41	1931	1070	3.15	1.38	43.3
2.41	1.41	2906	1048	5.6	2.23	59.4
32.2	1.41	3697	1036	8.6	3.39	68.7
37.7	1.41	4302	1021	10.6	4.12	71.4
45.1	1.41	5116	1006	12.6	4.84	70.6
50.8	1.41	5743	1000	14.6	5.53	72.3
58.1	1.41	6546	981	16.6	6.20	70.3
63.6	1.41	7151	976	18.6	6.91	72.20
71.6	1.41	8031	963	20.6	7.55	70.2







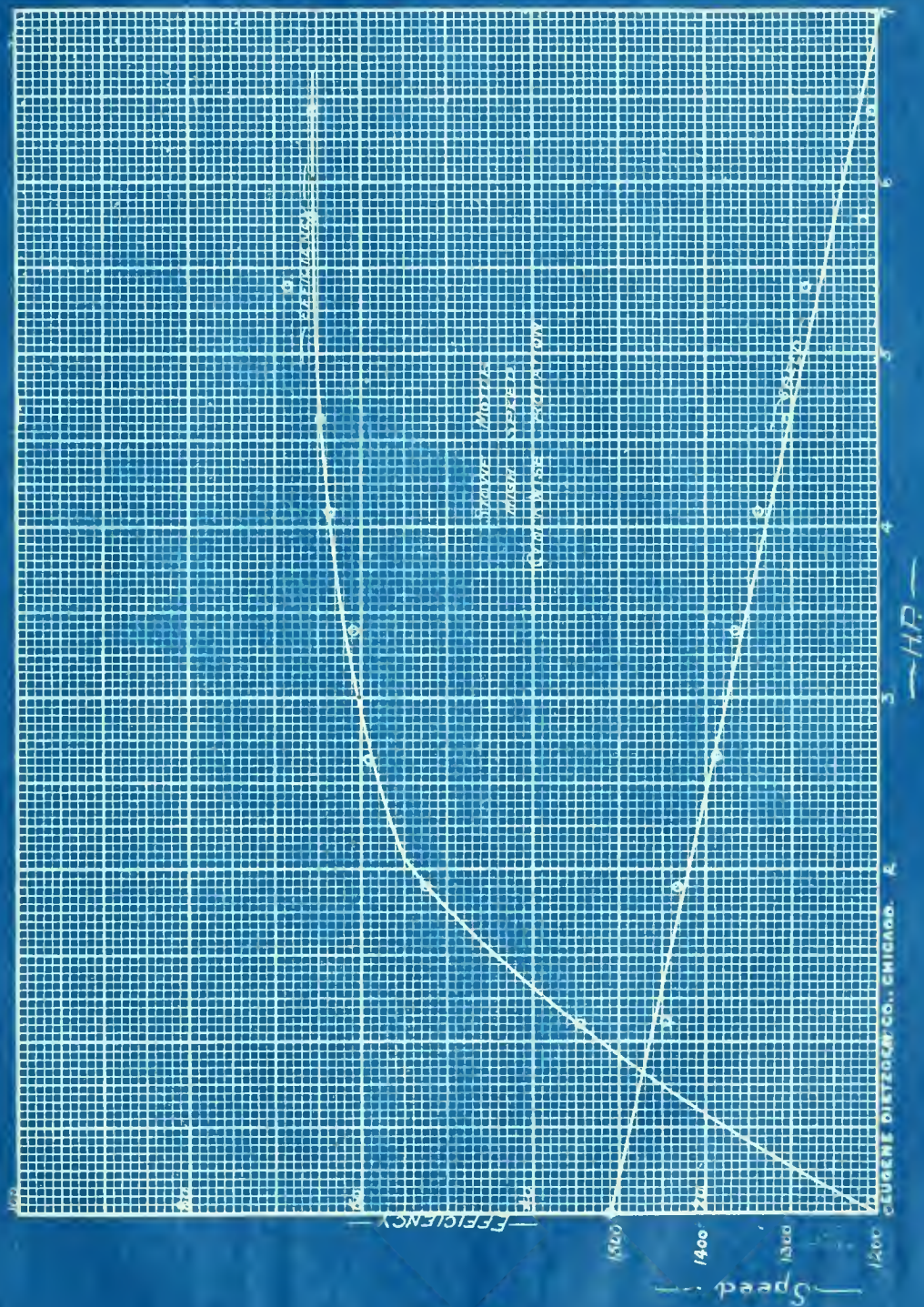


# Stowe Motor.

Ia.	If.	High Speed	Clockwise Rotation.			
		Watt Input	Speed	Wt.	H. P.	E.T.
12.1	1.33	1477	1510	0.	0.	0.
21.5	1.32	2510	1499	2.0	1.08	31.7
23.8	1.32	2735	1499	3.5	1.27	50.6
31.7	1.32	3632	1335	5.0	2.40	55.0
35.7	1.31	4071	1330	6.5	3.37	63.3
42.9	1.31	4835	1325	8.0	4.04	62.0
47.9	1.31	5413	1282	9.5	4.34	61.0
50.9	1.31	5743	1282	11.0	5.37	70.0
59.7	1.31	6711	1225	12.5	5.92	65.0
66.2	1.31	7423	1211	14.0	6.43	65.0
12.6	1.33	1532	1510	0.	0.	0.
19.7	1.33	2315	1474	2.0	1.12	51.2
22.8	1.31	2652	1457	3.5	1.24	51.5
27.6	1.31	3180	1409	5.0	2.68	45.0
32.1	1.31	4225	1373	6.5	3.4	40.0
41.3	1.3	4683	1354	8.0	4.13	35.7
43.8	1.3	5511	1325	10.5	4.79	34.0
53.0	1.3	5973	1289	11.0	5.40	37.5
53.1	1.3	6534	1200	12.5	5.72	30.5
64.1	1.3	7124	1193	14.0	6.37	31.0

E---110 Volts.







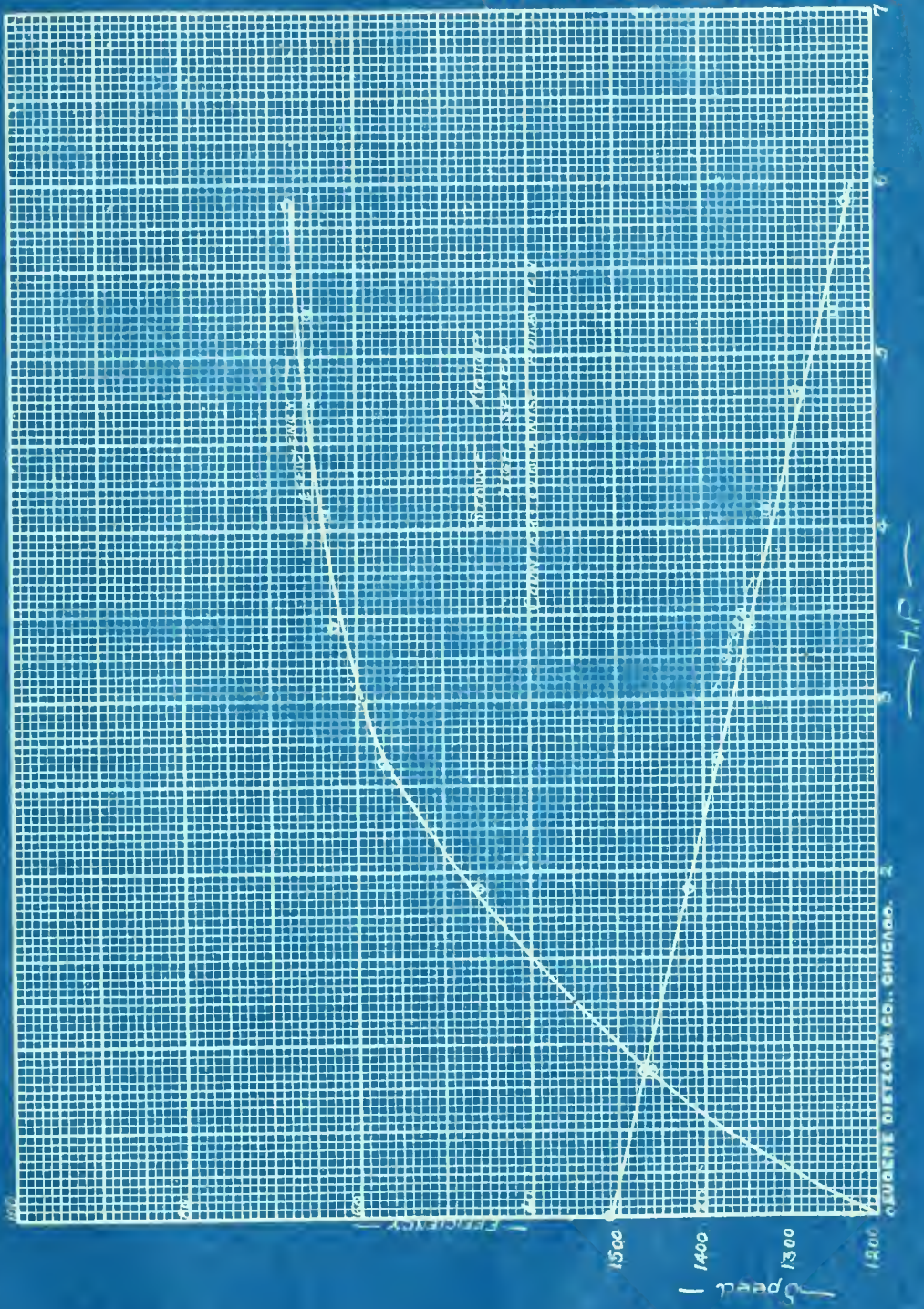


Stowe 6000.

M. S. Speed			Counter Circ. 150 Rev. 100 R.			
1a.	1f.	Watt Input	Speed	At.	H. .	Eff.
19.0	1.4	1474	1510	0.	0.	0.
20.1	1.4	2335	1474	3.	1.135	35.5
23.7	1.4	2731	1432	3.5	1.35	52.7
33.0	1.39	3732	1421	5.1	2.73	74.7
33.8	1.39	4420	1391	6.5	3.45	74.5
45.0	1.39	5102	1353	8.1	4.13	81.2
48.7	1.39	5502	1328	9.5	4.35	85.1
54.0	1.38	6021	1302	11.0	5.52	87.2
60.3	1.38	6317	1243	12.5	5.95	91.7
19.7	1.37	1543	1510	0.	0.	0.
19.6	1.37	2307	1432	1.5	0.54	37.
25.6	1.33	2967	1421	3.5	1.0	45.7
30.1	1.37	3431	1333	5.0	2.34	57.2
35.7	1.37	4077	1343	6.7	3.43	62.1
42.3	1.37	4303	1323	6.1	4.20	71.5
47.3	1.37	5353	1290	9.3	4.72	87.4
52.0	1.37	5930	1248	11.0	5.34	95.5
57.3	1.37	6503	1230	12.5	5.33	97.5

E-- 110 Volts.









Atone Motor.

Half Load (Constant) Clockwise Rotation.

Id.	If.	Watt Input	Speed	A. T.	A. P.	Eff.
25.7	1.37	2977	700	11.25	3.	75.2
26.3	1.36	3042	800	9.35	3.	77.5
29.2	1.36	3361	900	8.75	3.	83.3
30.9	1.36	3543	1000	7.37	3.	85.0
32.1	1.36	3700	1100	7.15	3.	89.1
34.2	1.36	3911	1200	6.55	3.	87.7
31.0	1.36	3559	1300	6.05	3.	82.2

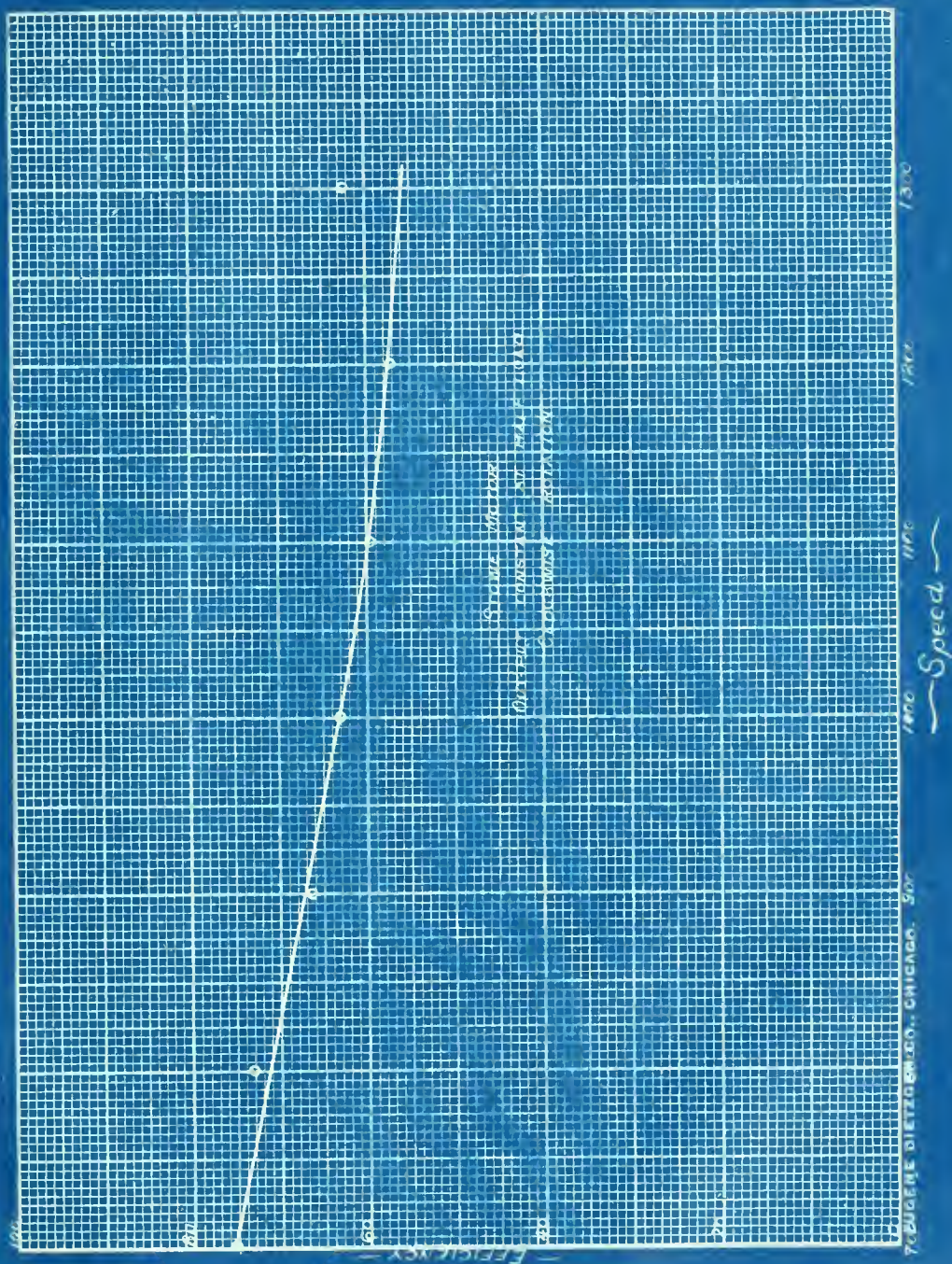
Half Load Constant

Counter Clockwise Rotation.

26.3	1.36	3042	700	11.25	3.	75.2
26.9	1.35	3107	800	9.35	3.	76.3
25.9	1.35	3107	900	8.75	3.	79.3
23.0	1.34	3227	1000	7.37	3.	85.4
30.6	1.34	3513	1100	7.15	3.	85.7
34.3	1.34	3953	1200	6.55	3.	86.3
33.3	1.34	4195	1300	6.05	3.	85.4
37.7	1.34	4294	1400	5.32	3.	82.2

E--- 110 Volts.









# Stowe Motor

Full Load (Constant) Clockwise Rotation.

Watt

Ia.	If.	input	Speed	Wt.	H. P.	Eff.
47.9	1.37	5464	700	22.5	6.	61.2
49.4	1.37	5594	800	19.7	6.	62.2
47.9	1.37	5464	900	17.5	6.	61.2
55.8	1.37	6388	1000	15.74	6.	71.2
53.8	1.37	6068	1100	14.3	6.	77.2
63.6	1.35	7144	1200	13.1	6.	82.7

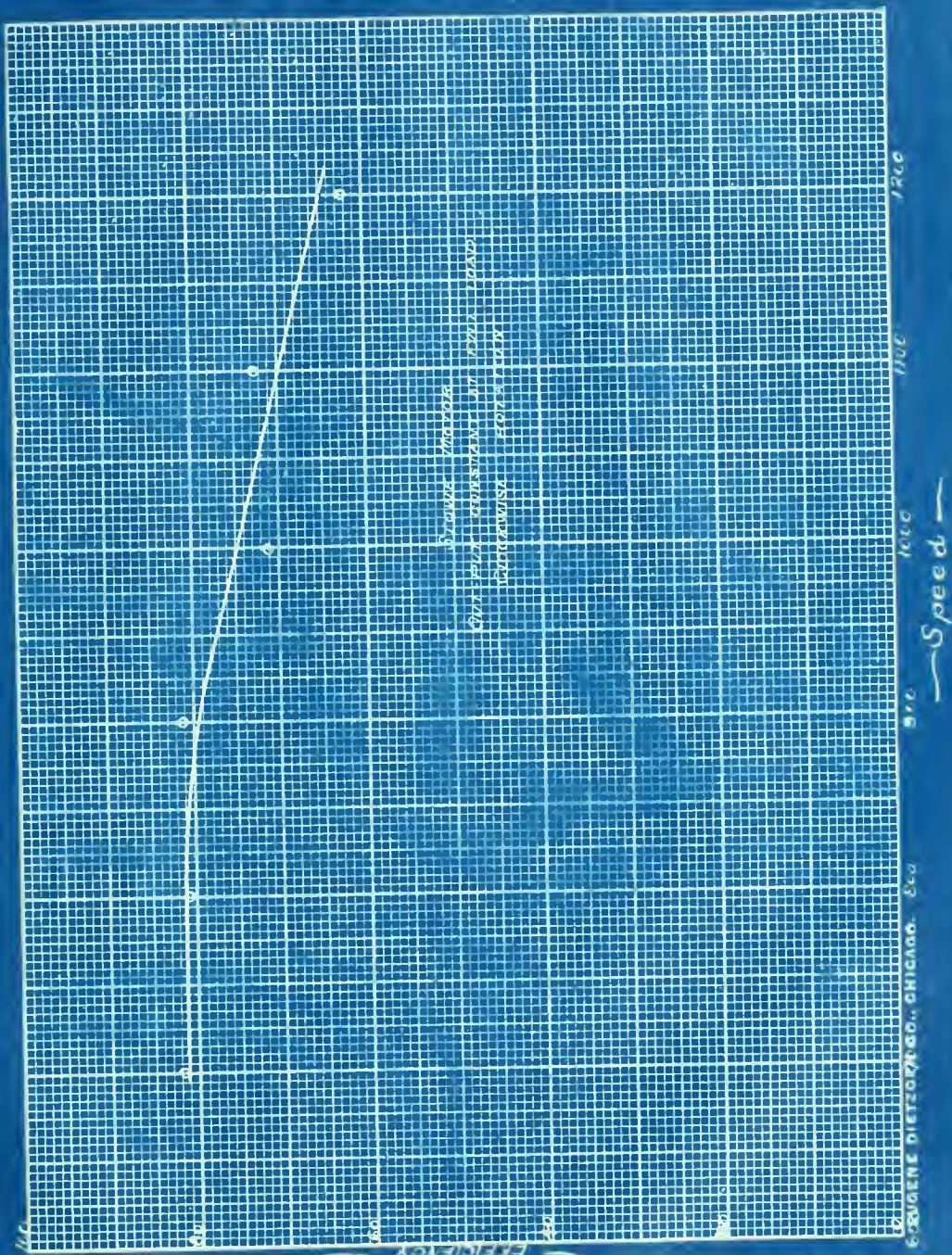
Full Load (Constant)

Counter Clockwise Rotation.

51.	1.4	5764	700	22.5	6.	77.0
53.6	1.39	6015	800	19.7	6.	74.4
57.9	1.38	6520	900	17.5	6.	68.3
62.1	1.37	6981	1000	15.74	6.	64.2
65.0	1.36	7299	1100	14.3	6.	61.4
67.0	1.35	7513	1200	13.1	6.	59.6

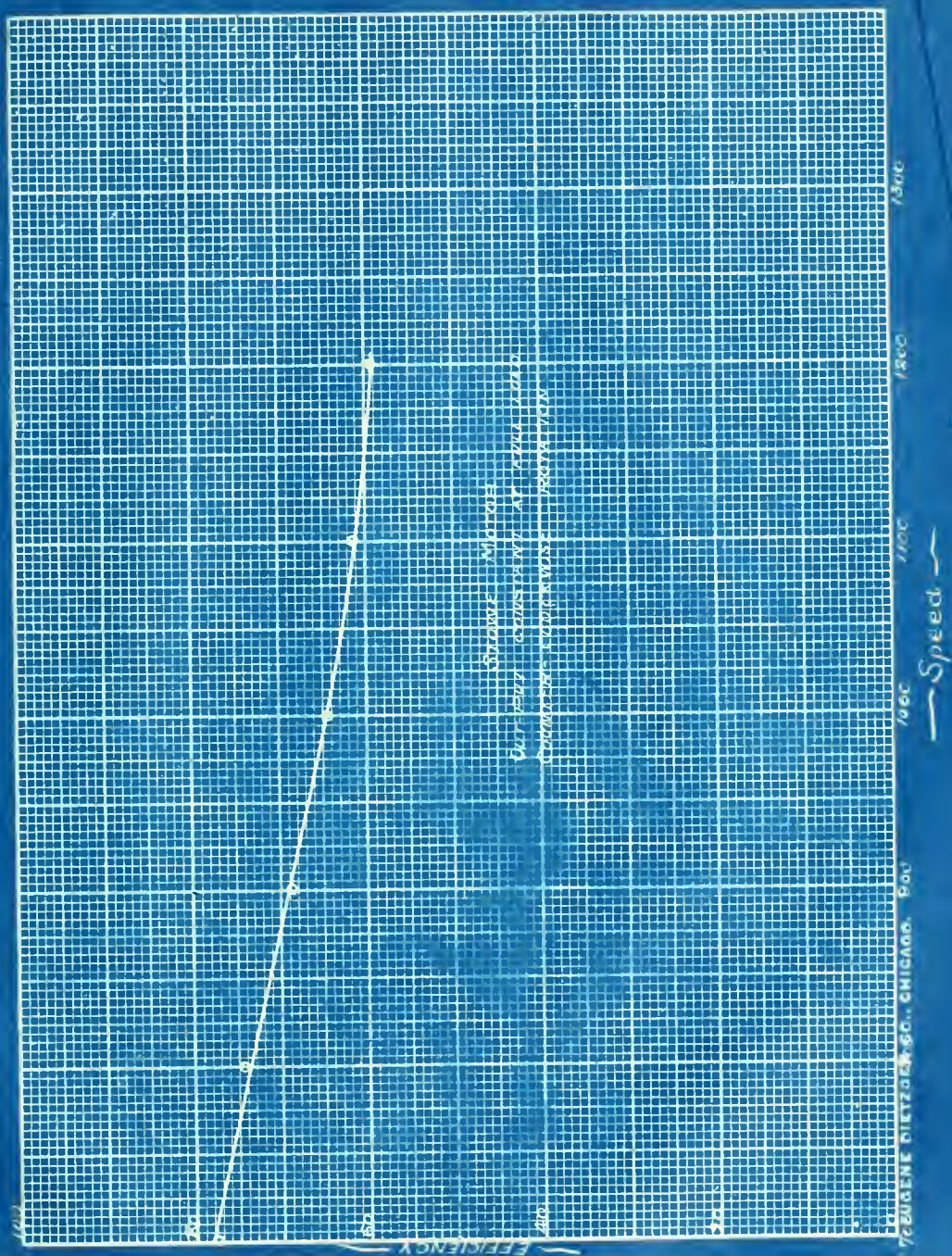
E-- 110 Volts.



















In the short-circuited coil, as the current flowing in it is reversed, passing from the maximum in one direction down to zero, and then up to the maximum in the opposite direction. The current thus varying in the coil induces a counter E.M.F. in the coil, which is due to the self-induction between coil turns. This counter E.M.F. is an active force tending to maintain the said varying current. The effect, therefore, of self-induction is to produce sparking.

The current flowing through the different armature coil produces a magnetic field in the space between the poles of the magnet, that is, in the region of the coil, that is, in the short-circuited.

These coils in their rotation, cut the lines of force of the field, and an E.M.F. is thereby generated in them. This E.M.F. is in such a direction that it tends to maintain the current flowing in the coil. The effect, therefore, of armature reaction is to produce sparking.

In the constant speed motor the two main causes of sparking are self induction of the short-circuited coil, and the action of this coil in generating & maintaining E.M.F. by cutting the field of the armature. These are overcome in part by the distance of the brush contact as mentioned above, and also by placing the brushes so that the short-circuited coil is in the edge of the main magnetic field. When properly placed the coil cuts lines of force in such a manner that the E.M.F. induced in the coil is the reverse of the counter E.M.F. that is, the main field is used to prevent the lines of force from the



field in the region of the short-circuited coil.

While it is possible in the present speed motor to control the sparking by the brush position alone, this method is entirely inadequate for the variable speed motor. The reduction of the field of strength necessary to obtain the high speeds, prevents its use in overcoming the magnetic field of the armature. The armature field is, therefore, not only present, but the increased speed of the armature proportionally increases the maintaining D. C. F. until it becomes so large that the carbon brush cannot overcome it. The increased speed of the armature also increases the E. M. F. of self-induction. As a result it becomes impossible for the carbon brush to reverse the current in the short-circuited coil, and in consequence there is destructive sparking at the high speeds. In order, therefore, to control these D. C. F. it is necessary to provide a magnetic field independent of the armature field. This is done in the present motor by two auxiliary coils, which are well connected with the main poles, and are placed between the latter as received with coil connected in series with the armature, so that all of the current flowing through the latter flows through the coils of the auxiliary field. These coils are wound on the same magnetic core as the main poles of the motor. The coils of the auxiliary field are connected in series with the armature, and the current in the









2. 11000 rpm, clockwise rotation: same curves as in (1).

For the intermediate pole the maximum efficiency was reached at about half load being 80.8% after which it dropped gradually. The speed regulation was 2.5-4% from zero to full load: the curve being a straight line.

The diode motor gave its highest efficiency at full load being 80.8% after which it dropped gradually. The speed regulation was 2.5-4% from zero to full load: the curve being a straight line.

The star gave an efficiency of 82% at full load, after which it dropped gradually. The speed regulation was 4.5% from zero to full load.

3. 11000 rpm, clockwise rotation: same curves as in (1).

For the intermediate pole the maximum efficiency was reached at about half load being 81.5%. From here it dropped gradually to 78.5% at full load. The speed dropped until half load was reached, then it rose to almost its normal value. The speed variation at half load was 4%.

The diode motor efficiency increased gradually to 80% at full load and remained practically constant to 50% half load. The speed regulation was 3% from zero to full load: the curve being a straight line.





The efficiency of the Lincoln motor at 1500 r.p.m. was 70% at half load, 75% at full load, and 78% at 50% overload. The speed regulation was 4.5% from half load to full load, the variation being in a straight line curve.

4. High speeds, clockwise rotation: curves as in (1).

For the motor at 1500 r.p.m. the efficiency was 70% at half load, 75% at full load, and 78% at 50% overload. The speed regulation was 4.5% from half load to full load, the variation being in a straight line curve.

The efficiency of the Lincoln motor at 1500 r.p.m. was 70% at half load, 75% at full load, and 78% at 50% overload. The speed regulation was 4.5% from half load to full load, the variation being in a straight line curve.

In the case of the efficiency is a maximum at full load being 72.8%. The efficiency at light loads was rather poor, that at a quarter load being 53%. The speed variation was in a straight line curve, the regulation being 9%.

5. High speeds, clockwise rotation: curves as in (1).

On the interpole the efficiency reaches its maximum at about half load, being 77.5%, gradually decreasing till at full load it is 75%. The efficiency at light loads are good, a quarter load being 72.5%. The speed regulation was 4.5%, the speed varying with the load to half load after which it was constant.

The efficiency for the Lincoln motor was 77.5% at half load, 70% at full load and at 50% overload 71.5%. The speed regulation was 8% from half load to full load.



The Stow gave an efficiency of 30% at quarter load, 35% at half load, and 40% at full load. The speed regulation was 22.5% from no load to full load; the curve being a straight line.

6. High speed counter clockwise rotation: curve (11)

In the Interpole the efficiency at quarter load was 25%, at half load 31% and at full load 36%. The speed regulation was 4.5% from no load to full load, the curve being a straight line.

The efficiency of the Lincoln motor was 50% at quarter load, 35% at half and from there constant to 50% overload. The speed regulation was 13%, the speed varying with the load.

In the Stow the efficiency at quarter load was 25%, at half load 50.3% and at full load 37.5%. The speed regulation was 10% from no load to full load: there being a straight line variation between load and speed.

7. Variation in efficiency with speed, the load constant at full load: clockwise rotation.

On the interpole motor the full load efficiency ran from 33.5% at 120 revolutions per minute to 75.5% at 1700 r.p.m. The curve is a straight line on the log speed scale, it is to drop a little above half speed and drops rapidly at low speeds.

The efficiency of the Lincoln motor ran from 31.5% at 300 r.p.m. to 72.5% at 1450 r.p.m. The variation followed a straight line.

The Stow had an efficiency of 31% at 700 r.p.m. and 35% at









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light loads, while the other, even at very light loads, is at light loads.

An example of the variation of the above is shown in the curves, this:

Low speed, clockwise rotation.

Load.	Int. revs.	Lincoln	Star.
1-4	75.7	34.5	61.7
1-2	32.2	74.5	72
3-4	34	72	73
Full	33.8	31	72.

Another striking variation can be seen from the high speed, clockwise rotation curves.

Load.	Int. revs.	Lincoln	Star.
1-4	72.5	50.7	44.7
1-2	73.4	37.5	60.5
3-4	73.2	39.3	34.7
Full	75.5	70.	35.5

The small variation of the appliances can be seen from the regulation, clockwise rotation curves.



Interpol.	Lincoln	Stow.
3 5-4%	10 2-3%	20%
High speed 4 1-2%	2%	20.5%

Another table will show the variation of efficiency with speeds.

Full load	Interpol.	Lincoln	Stow.
High speed	83.5%	87%	87%
High	73%	72%	65%

The motor range of speed of the Interpol. is 4 to 7, of the Lincoln 5 to 7, and of the Stow 2 to 7. The Interpol. has increased its full load speed from 1750 to 1800 r.p.m. giving a speed range of 3 to 7. The speed of the Lincoln

motor under full load gave a range of 4½ to 7. The Stow motor under full load gave a range of 1½ to 7.

All of the machines are direct, non-synchronous, outside armature series, although there is a marked difference in their mechanical construction. The Interpol. is of simple design, while the Lincoln and Stow, especially the former, possess a very complicated mechanical construction to obtain variable speed control.

As a result of our tests and observations we found the Interpol. motor superior to the Lincoln and Stow from the standpoint of high efficiency under average loads, and also from





tion, non-saturating and maximum loads, simple mechanical construction, and therefore concluded that the method of variable speed control, as embodied in the inter pole motor, is the best.

















